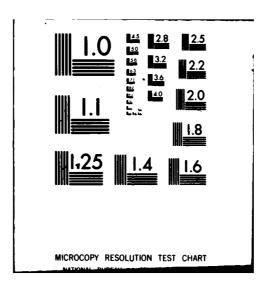
WOODWARD-CLYDE CONSULTANTS PLYMOUTH MEETING PA F/6 13/13 NATIONAL DAM INSPECTION PROGRAM. RAILROAD CREEK DAM (NDS ID NUM--ETC(U) AD-A082 668 JAN 80 M F BECK. J H FREDERICK DACW31-80-C-0018 UNCLASSIFIED NL 1 - 2 AL APPLICA



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DELAWARE RIVER BASIN

RAILROAD CREEK DAM
BUCKS COUNTY, PENNSTRANTA

(NDS I D NO+ PA 01062,
DER I D NO+ PA 615)
SCS NE PA 615)
PHASE I INSPECTION REPORT,
NATIONAL DAM INSPECTION PROGRAM

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15) DACW21-87-C-1117

Prepared by:

WOODWARD-CLYDE CONSULTANTS'
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Submitted to:

DEPARTMENT OF THE ARMY
Baltimore District, Corps of Engineers
Baltimore, Maryland 21203

JANUARY 1980

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#### PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams for Phase I Investigations. Copies of these guidelines may be obtained from the Office of the Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I investigation is to expeditiously identify those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigations, testing and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify the need for more detailed studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected, and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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# PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

Name of Dam: County Located: State Located: Stream:

Railroad Creek Dam Bucks County Pennsylvania

\_ ...

Unnamed Tributary to West Branch of Neshaminy Creek

Coordinates: Latitude 40° 17.2 Longitude 75° 14.0'

Date of Inspection: October 25, 1979

Railroad Creek Dam is owned by the Neshaminy Water Resources Authority and maintained by Bucks County. The dam and reservoir are used as a flood control structure for the downstream town of Chalfont, Pennsylvania. The impoundment was designed by the United States Department of Agriculture, Soil Conservation Service (SCS) in 1972 and 1973, and the structure was officially completed in 1977.

The dam and its appurtenant facilities are considered to be in good condition. The dam is classified as an "Intermediate" size structure with a "High" hazard classification, consistent with its potential in the event of failure for extensive property damage and loss of life in Chalfont, Pennsylvania.

Calculations indicate that the existing spillway systems are capable of passing the Probable Maximum Flood (PMF) without overtopping. Therefore, the spillway system is considered to be "Adequate".

The visual inspection and review of available documentation indicates that the dam, foundation and its appurtenant structures are in good condition and the embankment materials were placed in accordance with specification requirements. The vegetation is in poor condition, but no significant damage has resulted to the embankment itself. It was noted that the aluminum trash rack channels are bent and an angle bar is missing from the pond drain trash rack. An electric cattle fence is located along the upstream toe and berm of the dam and across the emergency spillway.

In addition to the annual maintenance of the structure, it is recommended that the following suggestions be implemented as specified. It is recommended that the following step be taken immediately.

The electric cattle fence should be moved upstream of the riser away from the embankment toe.

The following measures should be taken as soon as practical.

- 2. The vegetative cover on the embankment should be reestablished in a satisfactory manner.
- 3. The missing angle on the pond drain trash rack and the bolts on the embankment drain outlets should be replaced.

Because of the location of the dam upstream of Chalfont, a formal procedure of observation and warning during periods of high precipitation has been developed. The Owner also has an "Operations Manual" and maintenance procedures. It is important that individuals responsible for the maintenance and operation of Railroad Creek Dam are aware of the written procedures to insure that all items are carefully inspected and maintained on a periodic basis.

Mary F. Beck, P.E.

Feb. 7, 1980

Pennsylvania Registration 27447E

Woodward-Clyde Consultants

John H. Frederick, Jr., P.E. Maryland Registration 7301

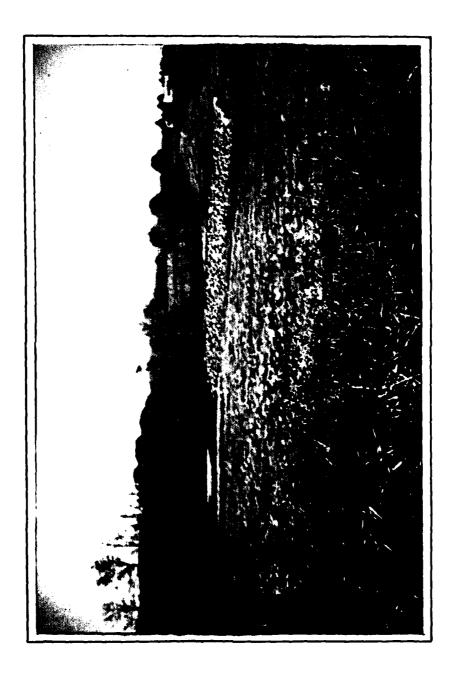
Woodward-Clyde Consultants

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APPROVED BY:

THOMAS A. RHEN

LTC, Corps of Engineers Acting District Engineer



OVERVIEW
RAILROAD CREEK DAM, BUCKS COUNTY, PENNSYLVANIA

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PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM
RAILROAD CREEK DAM
(SCS PA 615)
NATIONAL ID NO. PA 01062
DER NO. 9-175

# SECTION 1 PROJECT INFORMATION

#### 1.1 General.

- a. <u>Authority</u>. The Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of inspection of dams throughout the United States.
- b. <u>Purpose</u>. The purpose of the inspection is to determine if the dam constitutes a hazard to human life or property.

#### 1.2 Description of Project.

Dam and Appurtenances. Railroad Creek Dam is a 34 foot-high zoned earth embankment about 1,170 feet long with an emergency spillway at the left end of the embankment. The embankment contains an impervious core constructed over a cutoff trench under the dam centerline. The core and cutoff trench are composed of materials classified as silty clays and clayey silts (Zone 1) and encompassed by more permeable materials classified as silty gravels (Zone 2). The upstream slope is 3H:1V with a ten foot berm at approximately elevation The downstream slope is 2.5H:1V. The upstream and downstream slopes of the relatively impervious Zone 1 core are The embankment crest is 14 feet wide and has a 1.5H:1V. settled fill elevation of 292.2. Both upstream and downstream slopes are protected with Crownvetch. Embankment seepage is controlled by a trench drain near the downstream toe which contains 12 inch diameter perforated drain pipes that discharge through the impact basin sidewalls at the downstream Plan and cross-section views of the dam are shown on Plates 2 through 5, Appendix E, and embankment drainage details are shown on Plate 7.

The principal spillway consists of a concrete drop inlet riser, 202 feet of 30 inch diameter reinforced concrete, steel cylinder pressure pipe, with seven anti-seep collars and an impact basin at the downstream toe. The reservoir drain located at the base of the riser has an invert elevation of

- 258.75, and the elevation of the riser weirs is 267.5. The outlet invert and impact basin end sill elevations are 256.0. Because of high pressure gas lines which cross the reservoir area, the pond drain gate is not closed and water is not normally impounded behind the dam. Typical sections and details of the principal spillway are presented on Plates 8 through 13 in Appendix E. The emergency spillway is a trapezoidal channel excavated around the left end of the embankment. The 250 foot wide channel has side slopes of 3H:1V, and the 30 foot level section is at elevation 284.5.
  - b. Location. The dam is located on an unnamed stream, known locally as Railroad Creek, a tributary to the West Branch of Neshaminy Creek in New Britain Township, Bucks County, Pennsylvania. The dam is located approximately one mile west of Chalfont, Pennsylvania. The dam site is located on USGS Quadrangle entitled "Doylestown, Pennsylvania", at coordinates N 40° 17.2' W 75° 14.0'. A regional location plan of Railroad Creek Dam is included as Plate 1, Appendix E.
  - c. <u>Size Classification</u>. The dam is classified as an "Intermediate" size dam by virtue of its 1,610 acre-foot total storage capacity.
  - d. <u>Hazard Classification</u>. A "High" hazard classification is assigned consistent with the potential for extensive property damage and loss of life along the West Branch of Neshaminy Creek downstream of the dam.
  - e. Ownership. Railroad Creek Dam is owned by Neshaminy Water Resources Authority. All correspondence should be sent to Mr. William Taylor, Neshaminy Water Resources Authority, Post Office Box 6, Cross Keys Office Center, 4259 Swamp Road, Doylestown, Pennsylvania 18901.
  - f. Purpose of Dam. The purpose of this dam is flood control. The structure is one of ten dams in the Neshaminy Creek Watershed that are scheduled for construction with the assistance of the United States Department of Agriculture, Soil Conservation Service (SCS). This is the sixth project of the series.
  - g. Design and Construction History. The dam was designed by the SCS in 1972 and 1973. The application to construct a flood control dam and reservoir was submitted April 19, 1974. A letter of the same date from the Neshaminy Water Resources Authority to the Pennsylvania Department of Environmental Resources notes that, "in order to accommodate the requirements of the Texas Eastern Company gas transmission mains which cross the reservoir, the sedimentation pool will be left empty and there will not be a permanent water pool." The "Report upon the Application" was issued by the State of

Pennsylvania on January 14, 1976. The project was approved by the Delaware River Basin Commission in July of 1976, and construction began in early 1977 by Thomas Durkin & Sons. The dam was officially completed December 7, 1977.

Records in the Department of Environmental Resources files indicate that all work was performed in a satisfactory manner. Documents prepared by SCS personnel indicate that results of the in-place density test on the Zone 1 (core) material all exceed at least 95 percent of the Standard Proctor maximum density (ASTM D 698). Compaction of the Zone 2 (shell) material was by method specification requiring at least six passes with a 450 psi tamping roller per maximum 18 inch lift. Complete construction records are on file with SCS in Harrisburg.

The embankment was seeded during an exceptionally mild spell in late October 1977, toward the end of the seeding period. At least some of the seed germinated and was subsequently frozen during the following winter. SCS has prepared a reseeding plan to be implemented in the spring or early summer of 1980.

SCS is investigating replacement of aluminum trash rack channels with steel channels. The channels were bent by ice during the first winter when the reservoir level was high during a rapid freeze.

h. Normal Operating Procedures. Reservoir outflow is controlled by the principal and emergency spillways. Under normal conditions, water flows through the principal spillway. The pond drain gate is left open and no water is impounded behind the embankment. Excess water is stored up to the weir crest elevation, 267.5, and thereafter to elevation 284.5, the crest of the emergency spillway. Water is discharged through the emergency spillway at the left abutment only during storms with recurrence frequencies of once in 100 years.

#### 1.3 Pertinent Data.

A summary of pertinent data for Railroad Creek Dam is presented as follows.

a.	Drainage	Area	/ gamare	miles)	3.39
<b>a.</b>	Dialiage	wrea	Souge	m * T ← 2 \	2022

b.	Discharge at Dam Site (cfs) Maximum Known Flood at Dam	
	Site	Unknown
	Design High Water	2,290
	At Top of Dam	15,120

c.	Elevation (feet above MSL) Top of Dam Design High Water Emergency Spillway Crest Principal Spillway Weir Crest Pond Drain Inlet Invert Outlet Invert Downstream Toe	292.2 287.5 284.5 267.5 258.75 256.0 258.0
đ.	Reservoir (miles) Length at Normal Pool Length at Design High Water	Dry 0.9
e.	Storage (acre-feet) Sediment To Top of Dam	50 1,610
f.	Reservoir Surface Area (acres) Sediment Pool Design High Water	13 110
g.	Dam Data Type  Volume Length Maximum Height Top Width Side Slopes Upstream Downstream Cutoff  Grout Curtain	Zoned earth embank- ment 88,400 cu yds 1,170 feet 34 feet 14 feet  3H:1V 2.5H:1V Trench under center- line None
h.	Principal Spillway Type  Reservoir drain Elevation Weirs Pond Drain Inlet Invert Conduit Outlet Invert Energy Dissipator	Single stage reinforced concrete drop inlet riser, 30 inch conduit and impact basin At base of riser  267.5 258.75 256.0 Impact basin

Service Service

i. Emergency Spillway Type

> Width Side Slopes

Grass lined trapezoidal channel 250 feet 3H:1V

#### SECTION 2 ENGINEERING DATA

#### 2.1 Design.

- a. Data Available. A summary of the available engineering data on SCS PA 615, known as Railroad Creek Dam, is attached as Appendix B. Engineering data available for review is contained in a several hundred page design folder and a 37 page set of as-built plans. The design folder and plans are located in Soil Conservation Service (SCS) files and as-built drawings are also located in Department of Environmental Resources (DER) and the Owner's files. All of these records were prepared by the United States Department of Agriculture, Soil Conservation Service. Additional information was obtained from miscellaneous letters, correspondence and monthly construction reports in DER files.
- b. Design Features. The principal design features of Railroad Creek Dam are illustrated on the plans and profiles enclosed in Appendix E as Plates 2 through 13. A detailed description of the design features is also described in Section 1.2, paragraph a, and pertinent data relative to the structure is presented in Section 1.3. In addition to the plans of the dam, Plates 14 and 15 are enclosed to show the locations of the test borings and the results of typical compaction tests performed as part of the design.

#### 2.2 Construction.

Construction history is presented in Section 1.2, paragraph g. Construction records are located in DER and SCS files, and specific aspects of construction were obtained from the Neshaminy Water Resources Authority's representative and the SCS project engineer.

#### 2.3 Operational Data.

There are no operational records maintained. There are no minimum flow requirements for the downstream channel. There are no water level measurements or rainfall records maintained within the watershed although Neshaminy Water Resources Authority maintains a rain gauge at their office in Cross Keys, Pennsylvania.

#### 2.4 Evaluation.

- a. Availability. All engineering data evaluated and reproduced for this report were provided by either DER or SCS and supplemented by conversations and data obtained from representatives of the Neshaminy Water Resources Authority.
- b. Adequacy. Data included in State files, supplemented with data obtained from the Neshaminy Water Resources Authority and information received from State and Authority representatives, are considered adequate to evaluate the dam and appurtenant structures.
- c. <u>Validity</u>. There is no reason to question the validity of this data.

#### SECTION 3 VISUAL INSPECTION

#### 3.1 Findings.

- a. General. Observations and comments of the field inspection team are contained in the checklist enclosed herein as Appendix A, and are summarized and evaluated as follows. In general, the dam and its appurtenant structures are considered to be in good condition, with the exception of the vegetative cover to the embankment. At the time of the inspection, stream flow was passing through the riser of the principal spillway.
- b. <u>Dam.</u> During the visual inspection, there were no indications of distortion in alignment or grade that would be indicative of movement of the embankment or foundation. Vegetative cover on the embankment is considered in poor condition, with patchy areas, particularly at the maximum section. At the time of inspection, there was very little damage evident as a result of the poor vegetative cover. An electric cattle fence is located along the upstream toe and berm of the dam and across the emergency spillway. At the present time, no damage to the embankment has resulted. However, it is recommended that the fence be moved away from the embankment to prevent possible future damage from grazing cattle, particularly during a dry summer.

The vertical and horizontal alignments were checked and found to be satisfactory. Junctions between the embankment and abutment and the embankment and spillway were judged to be in good condition with no excessive erosion or deterioration. Clear seepage was observed entering the downstream channel below the impact basin from the right. An area to the left of the impact basin contains grass and vegetation indicative of a wet area. As the reservoir is dry, seepage is judged to be the result of hillside seepage. The upstream berm was wet and soft and appears not to drain well. Embankment drains outletting through the walls of the impact basin were dry.

#### c. Appurtenant Structures.

l. Principal Spillway. As shown on the plates, the riser is located at the upstream toe of the embankment. The exposed portions of the riser were inspected and evaluated to be in good condition with no signs of excessive concrete deterioration, spalling or other structural deficiency or defects. As shown in Photograph 9, an angle is missing from the pond drain trash rack. Photograph 8 shows that aluminum channels forming the upper stage trash rack are bent. The

channels were bent by ice during the winter of 1977-78. At the time of inspection, the low stage trash rack was clear of debris, although some debris was noted at the stream edge. By December, this debris had collected in the trash rack. The pond drain gate was exercised and was observed to seal completely. The impact basin at the downstream toe was inspected and found to be in good condition with no significant cracking or spalling of the concrete or erosion adjacent to the structure. The embankment drains outlet through walls of the impact basin. The bolts used as small animal guards were missing and should be replaced. The downstream channel was also inspected and found to be in good condition with no significant erosion or deterioration.

- 2. Emergency Spillway. The grass-lined emergency spillway at the left abutment was inspected and found to be stable and in good condition. Rainwater/hillside seepage was observed on the left side of the emergency spillway floor. Small trees and scrub brush was observed at the discharge end of the emergency spillway. The owners plan on having them removed shortly.
- d. Reservoir. At the time of the inspection, no water was impounded behind the embankment. The pond drain is open permitting base flow to pass through the principal spillway. The reservoir slopes are well vegetated to the stream's edge. Debris was observed along the stream.
- Downstream Channel. As shown on Plate 1, Appendix E, Railroad Creek flows eastward and empties into the West , Branch of Neshaminy Creek about 3,500 feet below the dam. About 0.75 miles below the confluence, the West Branch flows under U.S. Route 202 and through Chalfont before joining the North Branch. Two other dams also provide flood protection for Chalfont. Peace Valley Dam, which is on the North Branch of Neshaminy Creek, and Pine Creek Dam, built across Pine Creek, a tributary to the North Branch. Between Railroad Creek Dam and the West Branch, the stream's 20 foot wide channel is stable with a valley gradient of about 0.005. Where Route 202 crosses the West Branch of Neshaminy Creek, there are at least six homes or businesses subject to damage in the event of dam failure, including one gasoline station protected by a dike on Route 202. Upstream of Route 202 is one factory and at least one other house that would be damaged or flooded in the event of failure. Railroad Creek Dam, in conjunction with Peace Valley Dam and Pine Run Dam, was designed to protect Chalfont, a highly populated area, from Therefore, a "High" hazard classification is flood damage. justified for Railroad Creek Dam.

#### 3.2 Evaluation.

Inspection of the dam and appurtenant facilities disclosed no evidence of apparent past or present movement that would indicate existing instability of the dam, principal spillway or emergency spillway. The exposed portions of the riser and impact basin were inspected, and the principal spillway is judged to be in good condition, with bent trash rack channels and a missing angle iron from the pond drain trash rack noted. The emergency spillway is considered to be in good condition. The embankment is considered to be in good condition although the vegetation cover is poor. The overall condition of the dam is considered good.

# SECTION 4 OPERATIONAL PROCEDURES

#### 4.1 Procedures.

Operational procedures are discussed in some detail in Section 1.2. Operation of the dam does not require a dam tender. Under normal conditions, flow discharges through the pond drain and through the 30 inch conduit at the base of the embankment. Excess water is stored and then discharged over the principal spillway riser weirs and through the conduit. Additional excess water is then stored and discharged over the crest of the emergency spillway. As reported by the Owner's representatives, water has never flowed over the emergency Written operation and maintenance procedures used by Neshaminy Water Resources Authority are contained in "State of Pennsylvania Watersheds and Resource Conservation and Development Operation and Maintenance Handbook for Projects Installed with Assistance from the Soil Conservation Service" and specific procedures for each site are contained in the "Operations Manual" prepared by William G. Major Associates, Inc., June 1977.

#### 4.2 Maintenance of the Dam.

The dam is maintained by Bucks County personnel who periodically check the embankment, mow the grass and remove woody vegetation. As owner of the dam, Neshaminy Water Resources Authority monitors the maintenance performed and assists if possible. Neshaminy Water Resources Authority recently supplied CETA workers who removed debris from the reservoir area.

#### 4.3 Maintenance of Operating Facilities.

Maintenance of these facilities includes cleaning debris from the trash racks, lubricating the gate hoist and checking the structural integrity of the principal spillway system.

#### 4.4 Warning Systems In Effect.

A draft warning procedure, dated January 1980, has been prepared by the local Civil Defense office. The draft has been submitted to both the Neshaminy Water Resources Authority and the State Office of Civil Defense in Harrisburg for review.

#### 4.5 Evaluation.

It is judged that the current operating procedure, which does not require a dam tender, is a realistic means of operating the relatively simple control facilities at Railroad Creek Dam.

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The "Operations Manual" prepared by William D. Majors Associates, Inc., summarizes the control features and the responsible agency for operation and maintenance of each project within the Neshaminy Watershed constructed by 1977. Although the operational philosophy for a single-purpose flood control structure is contained in the manual, a "fact sheet" pertaining to Railroad Creek Dam is required. It is important that individuals responsible for the maintenance and operation of Railroad Creek Dam are aware of the written procedures to insure that all items are carefully inspected and maintained on a periodic basis.

### SECTION 5 HYDROLOGY/HYDRAULICS

#### 5.1 Evaluation of Features.

a. <u>Design Data</u>. The complete folder of design calculations was reviewed, and portions of this folder are presented in Appendix C.

The watershed is about 2.5 miles long, and from 0.8 to 2.2 miles wide, having a total area of approximately 3.39 square miles. Elevations range from 660 in the upper reaches of the watershed to about 258.8 at the pond drain inlet elevation. The watershed is predominantly open/farmland, with less than 10 percent residential development. Residential development can be expected to progress rapidly.

In accordance with criteria established by Federal (OCE) Guidelines, the recommended spillway design flood for this "Intermediate" size dam and "High" hazard classification is the Probable Maximum Flood (PMF). The Soil Conservation Service designed this dam as a Class C structure, which requires that the spillway systems be designed to pass the PMF.

- b. Experience Data. There are no records of reservoir levels kept for this dam. Rainfall is measured and records are kept at the Neshaminy Water Resources Authority's office in Cross Keys, Doylestown, Pennsylvania. There are no estimates or records of previous high water levels.
- c. <u>Visual Observations</u>. On the date of the inspection, there were no conditions observed that would indicate a reduced spillway capacity during an extreme event. Observations regarding the condition of the downstream channel, spillways and reservoir are located in Appendix A and are discussed in greater detail in Section 3.
- d. Overtopping Potential. The dam was designed to pass the PMF without overtopping. The PMF inflow hydrograph and flood routing were done according to procedures in the SCS National Engineering Handbook. The flood routing was originally done by a graphical procedure. Subsequently, after land rights for the structure had been obtained, the flood routing was checked by the SCS computer program, TR-20, the results of which are included in Appendix C. The computer routing indicated a top of dam of 292.87 feet, about 0.7 foot higher than the current elevation. As land rights were obtained before the computer routing was performed, it was decided to lower the emergency spillway elevation by 0.5 foot and to retain the original flood routing as a basis for design.

Because of the differences in the flood routing by TR-20, the spillway adequacy was evaluated as part of this investigation according to standards established for the National Dam Overtopping potential of the dam was Inspection Program. estimated using the HEC-1, Dam Safety Version, computer A brief description of the program is included in program. Appendix D. Calculations for this investigation confirm the original design spillway discharge of about 15,000 cfs with the reservoir at the top of the embankment. The HEC-1 program computed the peak PMF inflow to be about 10,260 cfs. As the spillway capacity is greater than the computed peak PMF inflow, flood routing was not necessary. Spillway systems for this dam are considered to be "Adequate" as the dam will pass the PMF without overtopping.

Downstream Conditions. Downstream conditions and damage centers have been discussed in Section 3. In general, Railroad Creek Dam, together with Peace Valley Dam and Pine Run Dam controlling the upper reaches of the North Branch of Neshaminy Creek, provides relief from flooding in a rapidly urbanizing area. However, the SCS Neshaminy Watershed work plan concludes that a high potential for flood damage still exists downstream of these structures in Chalfont. estimated that damage from flooding has been reduced but not eliminated through control of the upper reaches of Neshaminy Watershed by flood control structures. In conclusion, it is evaluated that a significant increase in downstream damage would result from failure of the dam during a PMF than damage resulting from large flows during passage of the PMF.

### SECTION 6 STRUCTURAL STABILITY

#### 6.1 Evaluation of Structural Stability.

a. <u>Visual Observations</u>. Visual observations detected no evidence of existing or pending embankment instability. Upstream and downstream slopes appear stable, with no surficial slides or indications of deep seated instability. Both the upstream and downstream slopes are poorly vegetated with Crownvetch and require reseeding. There are no exterior signs or other evidence to indicate that the internal drainage systems were not operating properly. It is noted, however, that during this inspection, the reservoir was empty and the embankment was not retaining a significant head of water which could affect the internal drainage system.

Seepage and wet areas were observed at the down-stream toe. However, as there was no water behind the embankment, the seepage and wet areas are judged to be the result of hillside seepage rather than seepage through or under the embankment.

Exposed portions of the principal spillway were inspected and judged to be in good condition. The emergency spillway was also inspected and assessed to be in good condition.

b. Design and Construction Data. Design documentation is very complete as a several hundred page design folder prepared by the Soil Conservation Service (SCS) was available and reviewed at their office for this investigation. Data included in these files are a foundation report containing permeability test results, shear strength test results and a stability analysis, structural calculations for the principal spillway and a complete set of hydrologic/hydraulic calculations. Portions of the Hydrology/Hydraulics section are presented in Appendix D. Principal features of this structure are presented in the drawings located in Appendix E. Also included in the design folder are a complete set of specifications and an estimate of the quantity of material used in the embankment.

A stability analysis of the embankment was performed by SCS using the ICES-LEASE computer program. Soil parameters were based upon a total of five consolidated-undrained triaxial compression tests, with pore pressure measurements, conducted on compacted Zone 1 and Zone 2 embankment materials. The foundation materials were assumed to have sufficient strength to prevent potential failure arcs from passing through the foundation. The shear strength parameters adopted

for design were reviewed and are judged to be conservative, based on the test results. Stability analyses using the Swedish circle method resulted in the following minimum factors of safety:

Slope	Condition	Minimum Factor of Safety
Upstream	Rapid Full Drawdown	1.51
Downstream	Steady Seepage	1.52

The recommended allowable factors of safety for these conditions, in accordance with Corps of Engineers EM 1110-2-1902 are 1.2 and 1.5, respectively.

It is noted that the phreatic line assumed for the stability analysis corresponds to that which would occur for a homogeneous embankment. Since the embankment actually contains a relatively impervious core, the actual phreatic line would be higher on the upstream side and lower on the downstream side. This would cause an increase in the downstream (steady seepage) factor of safety and a decrease in the upstream (rapid drawdown) factor of safety. Since the upstream factor of safety is well above minimum, this decrease is not considered critical. Furthermore, the steady state and drawdown water level was assumed to be elevation 284.5, the emergency spillway crest elevation, rather than the highest principal spillway crest elevation, 267.5, as specified by current SCS criteria in TR-60. Therefore, it is concluded that the stability of the embankment is adequate.

Documents pertaining to construction also include a 37 sheet set of drawings prepared by the SCS and stamped "asbuilt". The progress reports prepared by the SCS resident engineer and inspection reports prepared by DER representatives indicate that work was performed in accordance with SCS requirements and that all in-place density test results exceeded the minimum specification of 95 percent of the Standard Proctor maximum density as defined by ASTM D 698.

- c. Operating Records. There are no operational records for this structure.
- d. <u>Post-Construction Changes</u>. There are no reports, nor is there any evidence, that modifications were made to this dam.
- e. <u>Seismic Stability</u>. The dam is located in Seismic Zone 1. Normally it can be considered that if a dam in this zone is stable under static loading conditions, it can be

assumed safe for any expected earthquake conditions. As the stability analysis resulted in a minimum factor of safety of 1.51 during rapid drawdown, the most critical loading condition, it can be assumed that seismic stability requirements are satisfied.

## SECTION 7 ASSESSMENT/REMEDIAL MEASURES

#### 7.1 Dam Assessment.

- a. Evaluation. Visual inspection and review of design and construction documentation indicate that the dam, foundation and appurtenant structures of Railroad Creek Dam are in generally good condition. The hydrologic and hydraulic computations presented in Appendix D indicate that the structure will pass the Probable Maximum Flood without overtopping. Therefore, the spillway systems of this structure are considered to be "Adequate". In the event that high flows are passed through the emergency spillway, significant property damage is still likely to occur along the West Branch of Neshaminy Creek and especially in the town of Chalfont, Pennsylvania, where there are many homes on or near the flood plain. In the event the dam fails while retaining a significant quantity of water, extreme property damage and possible loss of life would be expected.
- b. Adequacy of Information. The information available for this investigation was sufficiently adequate to evaluate the structural and hydraulic aspects of the dam.
- c. <u>Urgency</u>. It is recommended that the suggestions presented in Section 7.2 be implemented as specified.

#### 7.2 Remedial Measures.

- a. <u>Facilities</u>. It is recommended that the following step be taken immediately.
  - 1. The electric cattle fence should be moved upstream of the riser away from the embankment toe.

The following measures should be taken as soon as practical.

- 2. The vegetative cover on the embankment should be reestablished in a satisfactory manner.
- 3. The missing angle on the pond drain trash rack and the bolts on the embankment drain outlets should be replaced.
- b. Operation and Maintenance Procedures. Neshaminy Water Resources Authority has an "Operations Manual" specifying agencies responsible for operation and maintenance for Neshaminy Watershed projects completed by 1977. The manual requires updating to include Railroad Creek Dam. The

Operations Manual refers to "Development Operation and Maintenance Manual" prepared by SCS for a maintenance inspection checklist, which should be used to insure that all items are periodically inspected and maintained in the best possible condition. It is recommended that these procedures provide for a period of observation during and following impoundment of significant quantities of water behind the embankment. These observations should include monitoring discharge from the embankment drainage system and looking for sources of uncontrolled seepage.

A warning system has been drafted and is in the process of review. This warning procedure should include monitoring of the dam during periods of high precipitation and a method of warning and evacuating residents along the creek, if necessary.

APPENDIX

A

CHECK LIST VISUAL INSPECTION PHASE I

Sheet 1 of 11

Name: Dam Railroad Creek Dam	County Bucks	s State Pennsulvania	National ID # PA 01062
Lynn of Dam Fronth		Category	
125/79	Weather Clear	nperati	
Insuport	<u> </u>  -	Tailwater at Time of Inspection	M.S.L.
	1		
Inspection Personnel:			
Mary Beck (Hydrologist)	Vincent McKeever (Hydrologist)	rologist)	The second secon
Arthur Dvinoff (Geotechnical)			
Raymond S. Lambert (Geologist) 11/30/79	Mary F. Beck	ok	

# Remarks:

Mr. Eugene McGough of William D. Majors Associates. Inc., were on site and provided assistance to the inspection team. Messrs. Brent Wiggins and Bob Harbine of the local Civil Defense. Unit were also on site. Messrs. William Taylor and Charles Burger of the Neshaminy Water Resources Authority and

# CONCRETE/MASOHRY DAMS

VISUAL EXAMINATION OF	OBSERVATIONS	Sheet 2 of 11 REMARKS OR RECOMMENDATIONS
AUV NOFICEABLE SFEPAGE	N/A	
STRUCTURE TO ABUTHENT/CHRANKHLNT JUNCTIONS	N/A	
UKATAS	N/A	
WATER PASSAGES	N/A	
FORIGIDATION	N/A	

# CONCRETE/MASONIRY DAMS

VISUAL EXAMINATION OF	OBSERVATIONS N / A	REMARKS OR RECOMMENDATIONS
CINCRETE SUIFACES		
STRUCTURAL CRACKING	N/A	
VERTICAL AND HORIZONTAL	N/A	
MARIOL 1711 JOHNTS	N/A	

N/A

CONSTRUCTION JOINTS

		Sheet 4 of 11
VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SURFACE CRACKS		
None o	None observed.	

CRACKING AT OR BEYOND THE TOE

None observed.

SLOUGHING OR EROSTOR OF ENDANGIENT AND ABUTHENT SLOPES

Vegetation is sparce along the crest and on both upstream and downstream slopes at maximum section. Reseeding required. Almost no damage has resulted as a result of lack of vegetation. Slight damage (one set of tracks) made by truck or similar vehicle on upstream face near riser.

VERTICAL AND KORTZONTAL ALIGAMENT OF THE CREST

The vertical and horizontal alignment was checked and found to be satisfactory.

RIPHAP FAILURES

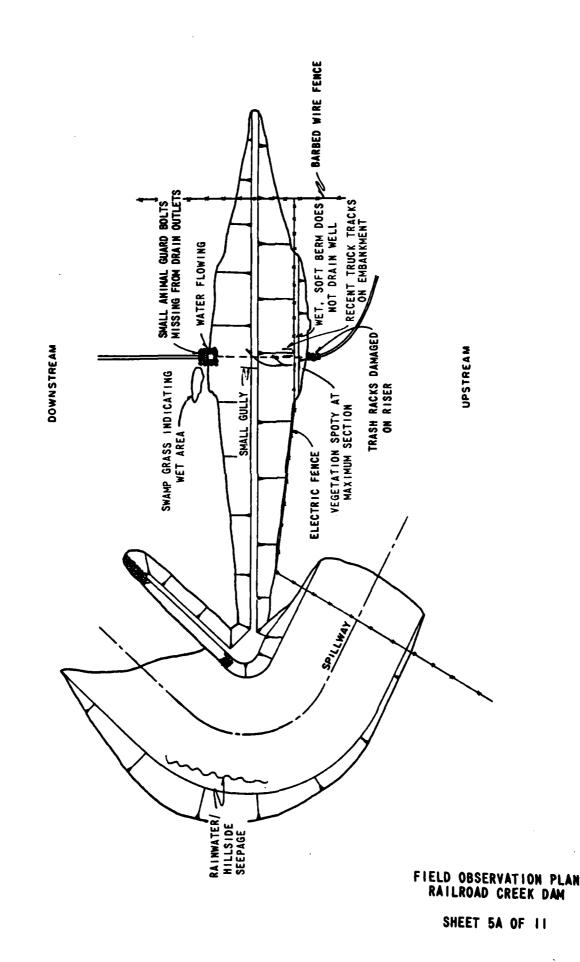
N/A

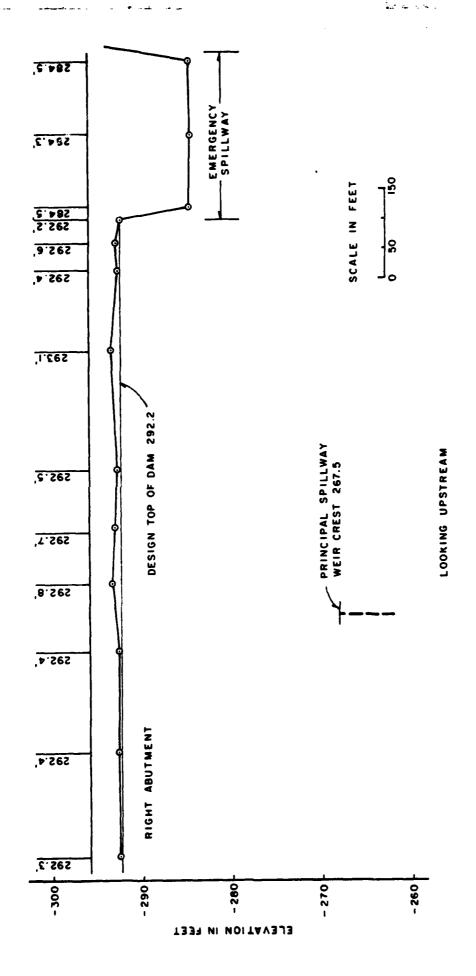
# EMBANKMENT

VISUAL EXAMINATION OF	Sheet 5 of 11 0BSERVATIONS REMARKS OR RECOMMENDATIONS
MISCELLANEOUS	An electric fence at the upstream toe and berm of the embankment allows cattle to graze in the reservoir and part of the emergency spillway. Currently, little or no damage has resulted from cattle traffic but damage is possible, particularly during a dry summer. It is recommended that the fence be moved away from the embankment toe.
JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLMAY AND DAM	All junctions of embankment and abutments in good condition.
ANY NOTICEABLE SEEPAGE	None, dry reservoir, see Sheet 5A.
STAFF GAGE AND RECORDER	None

DRAINS

Dry, bolts (small animal guards) missing, should be replaced.





FIELD OBSERVATION PROFILE RAILROAD CREEK DAM

SHEET 58 OF 11

# PRINCIPAL SPILLWAY OUTLET MORKS

Sheet 6 of 11

Andreas and the state of the st	Sheet 6 of 11
VISUAL EXAMINATION OF	OUSENVATIONS REMARKS OR RECOMMENDATIONS
CKACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT	Conduit is underground and could not be inspected.
IMTAKE STRUCTURE	Good, trash rock channels bent, reportedly from ice. One angle is missing from pond drain trash rack.
OUTLET STRUCTURE	Good condition, bolts (small animal guards) missing from embankment drain outlets (through side walls).
OUTLET CHARBEL	The channel immediately below the impact basin is in good condition.
LMERGLNCY GATE	Operates easily and seats completely.

# EMERGENCY SPILLWAY

# UNGATED SPILLWAY

REMARKS OR RECOMMENDATIONS Sheet 7 of 11 Good condition. Small trees and scrub brush at end of discharge channel. Owners plan on having them removed shortly. Spillway is a grass-lined trapezoidal channel. **OBSERVATIONS** Good condition. None VISUAL EXAMINATION OF DISCIMRGE CINIMEL CONTROL SECTION APPROACH CHANNEL BRIDGL AND PIERS

## CATED SPILLWAY

		Sheet 8 of 11
VISUAL EXAMINATION OF	OBSERVATIONS REPARKS OR RECOMPLINIATIONS	H NDAT LONS
CONCRETE SILL	N/A	
APPROACH CHAINEL	N/A	
DI SCHARGL CHANALL	N/A	
BRITIGE AND PILKS	N/A	
		!

and the second second

N/A

CATES AND OPERATION LIQUIPMENT

ţ.,

# INSTRUMENTAT 10N

VISUAL EXAMINATION	OBSERVATIONS RECOMMENDATIONS
PORUMENTALION/SURVEYS	No monuments installed, a post-construction survey of dam crest is included in Appendix E.
OBSERVATION WELLS	None
WE TRS	None
PIEZOMETERS	None
отитя	None

· ·

## RESERVOIR

VISUAL EXAMINATION OF	OBSERVATIONS	Sheet 10 of 11 REMARKS OR RECORMENDATIONS
SI.OPES	Reservoir side slopes are flat to moderate. trees and grass.	Well vegetated with

No sedimentation observed.

SEDIMENTATION

# DOWNSTREAM CHANNEL

Sheet 11 of 11

REMARKS OR RECOMMENDATIONS

VISUAL EXAMINATION OF OBSERVATIONS

CONDITION (OBSTRUCTIONS, DEBRIS, ETC.)

The 12 foot wide channel meanders through a wooded flood plain. Channel sides range from 8H:1V on inside of bends to nearly vertical on the cutting side.

SLOPES

The valley gradient is approximately 0.005.

APPROXIMATE NO. OF HOMES AND POPULATION

About 3,500 feet below the dam, Railroad Creek enters the West Branch of Neshaminy Creek. About 0.75 mile below the confluence, the West Branch flows under U.S. Route 202 and through Chalfont before joining the North Branch. In Chalfont there are at least six homes/businesses subject to damage in the event of dam failure, including one gas station protected by a dike on Route 202.

APPENDIX

B

CHECK LIST
ENGINEERING DATA
DESIGN, CONSTRUCTION, OPERATION
PHASE I

Railroad Creek Dam NAME OF DAM

PA 01062 # 91

ITEM

REMARKS

Sheet 1 of 4

AS-BUILT DRAWINGS

Drawings presented in Appendix E are "As-Built" drawings.

REGIONAL VICINITY MAP

See Plate 1, Appendix E.

CONSTRUCTION HISTORY

See Section 1.2 of text.

TYPICAL SECTIONS OF DAM

See Appendix E.

**OUTLETS - PLAW** 

DETAILS

CONSTRAINTS

DISCHARGE RATINGS

See Appendix D.

See Appendix E.

RAINFALL/RESERVOIR RECORDS

Rainfall is measured by Neshaminy Water Resources Authority at their office in Cross Keys about six miles northeast of the dam.

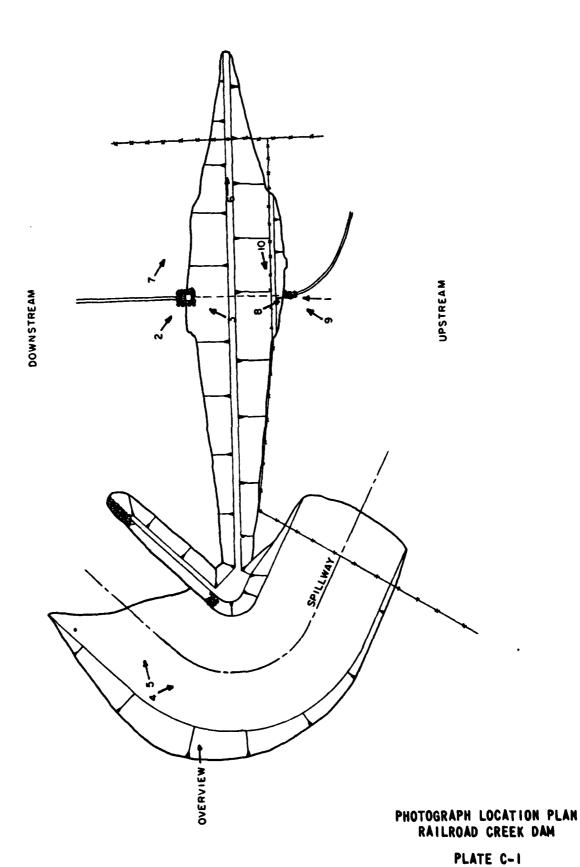
	Sheet 2 of	2 of
ITEM	REMARKS	
DESIGN REPORTS	See discussion in Section 1 of text.	
GEOLOGY REPORTS	See Appendix F.	
DESIGN COMPUTATIONS HYDROLOGY & HYDRAULICS UAM STABILITY SEEPAGE STUDIES	See discussion in Sections 5 and 6 of text.	
MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD	Complete records in SCS files.	
POST-CONSTRUCTION SURVEYS OF DAM	A final crest profile survey was performed. Data is presented on Plate 6, Appendix E.	
BORROW SOURCES	Data located on SCS drawings.	

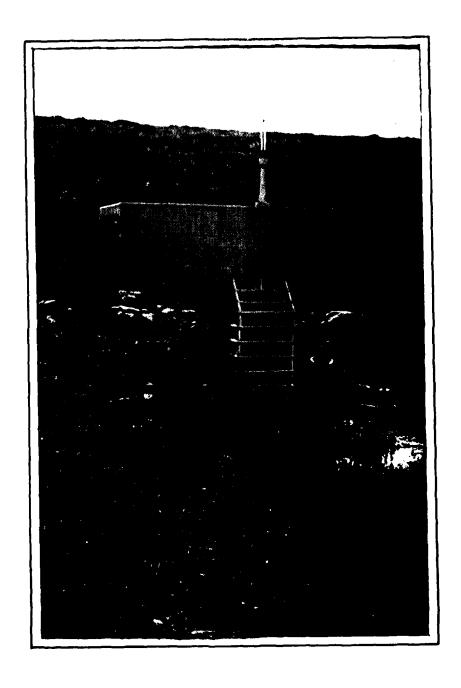
ITEM	Sheet 3 of 4 REMARKS
MÜMITURING SYSTEMS	None
MODIFICATIONS	All pertinent modifications are noted on the "As-Built" dravings presented in Appendix E.
HIGH POOL RECORDS	None
POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS	None
PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS	None
PAINTE: JANCE OPERATION RECORDS	Neshaminy Water Resources Authority maintains these files.

ITEM	REMARKS
SPILLWAY PLAN SECTIONS DETAILS	See Appendix E for details.
OPERATING EQUIPMENT PLANS & DETAILS	See Appendix E for details.
MISCELLANEOUS	1. Report Upon the Application of the Neshaminy Water Resources Authority submitted by the State of Pennsylvania, January 14, 1976.  2. Permit issued by State of Pennsylvania, January 21, 1976.  3. 37 design drawings prepared by SCS, 1973-1874.  4. Erosion and Sediment Control Plan prepared by SCS, September, 1974.  5. Progress Reports by Frederick Schuetz, Project Engineer, SCS.  6. Inspection Report prepared by the State.  7. 29 color photographs taken by DER Inspectors.  8. Special Operation and Mair tenance Report by SCS, August 15, 1978.

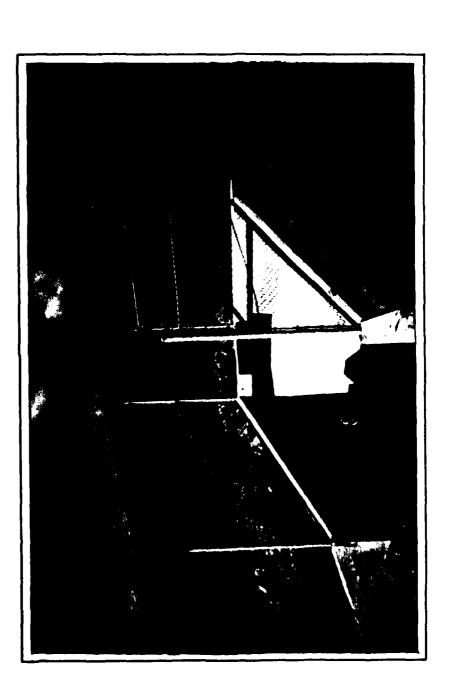
A PPENDIX

C

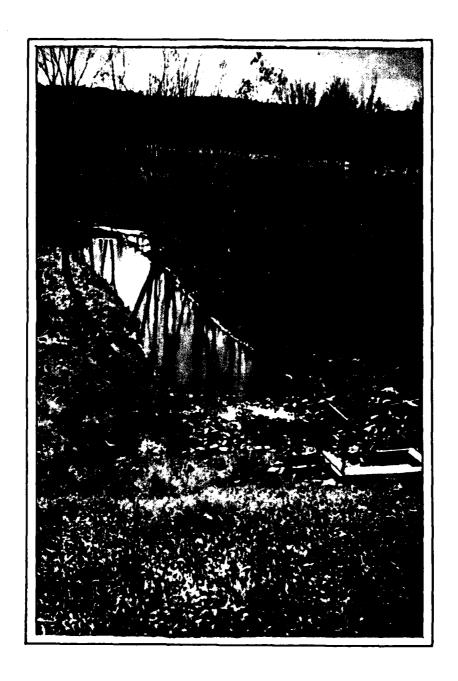




PRINCIPAL SPILLWAY RISER WITH OPEN POND DRAIN GATE.



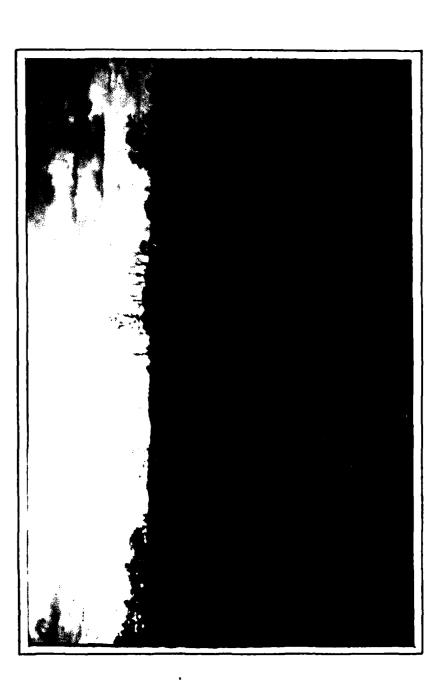
PRINCIPAL SPILLWAY IMPACT BASIN.
BOLTS (SMALL ANIMAL GUARD) ARE
MISSING FROM EMBANKMENT DRAIN
OUTLETS.



VIEW FROM TOP OF DAM SHOWING IMPACT BASIN AND DOWNSTREAM CHANNEL.

VIEW OF EMERGENCY SPILLWAY FROM LEFT ABUTMENT LOOKING UPSTREAM.

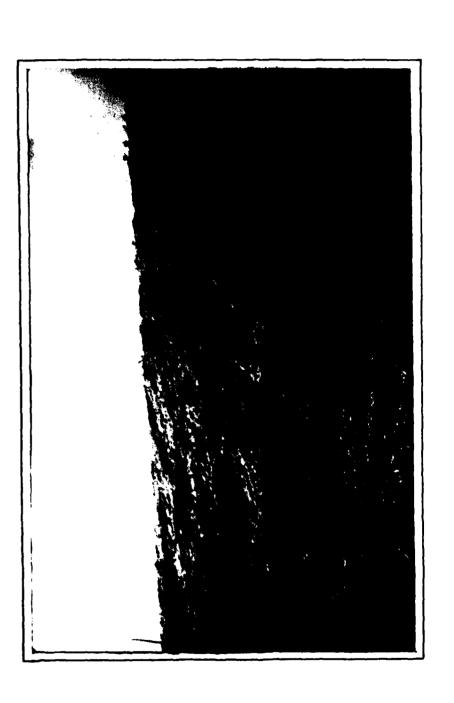
PHOTOGRAPH NO. 4



VIEW OF EMERGENCY SPILLWAY FROM LEFT ABUTMENT LOOKING DOWNSTREAM.



VIEW OF CREST, MINOR DAMAGE TO CREST FROM TRUCK TRAFFIC



OVERVIEW OF DOWNSTREAM SLOPE. NOTE FENCE POSTS AT CREST OF DAM.



TRASH RACK CHANNELS, REPORTEDLY DAMAGED BY ICE.



POND DRAIN TRASH RACK WITH MISSING ANGLE.



ELECTRIC FENCE AT UPSTREAM TOE.

SECOND DOWNSTREAM HIGHWAY BRIDGE AND DAMAGE CENTER. PICTURE TAKEN FROM DIKE PROTECTING GASOLINE STATION TO THE RIGHT OF THE PICTURE.

PHOTOGRAPH NO. 11

APPENDIX

D

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## RAILROAD CREEK DAM CHECK LIST HYDROLOGIC AND HYDRAULIC ENGINEERING DATA

DRAINAGE AREA CHARACTERISTICS: About 25% wooded, less than 10% residential,
remainder is open/farm land.
ELEVATION TOP NORMAL POOL (STORAGE CAPACITY): 267.5 feet (50 Acre-Feet).
ELEVATION TOP FLOOD CONTROL POOL (STORAGE CAPACITY): 292.2 feet (1610 Acre-Feet).
ELEVATION MAXIMUM DESIGN POOL: 287.5 feet Design High Water.
ELEVATION TOP DAM: 292.2 feet.
EMERGENCY SPILLWAY:
a. Elevation <u>284,5 feet.</u>
b. Type <u>Grass lined trapezodial chammel.</u>
c. Width <u>250 feet.</u>
d. Length <u>About 800 feet.</u>
e. Location Spillover At left abutment
f. Number and Type of Gates <u>None</u>
PRINCIPAL SPILLWAY:
a. Type Drop inlet riser, 30-inch conduit and impact basin.
b. Location Dom station 19+90, at maximum section.
c. Entrance inverts Riser weirs at 267.5 feet.
d. Exit inverts 256.0 feet.
e. Emergency draindown facilities <u>Pond drain inlet at 258.75 feet.</u>
HYDROMETEOROLOGICAL GAGES:
a. Type <u>Standard rain gage.</u>
b. Location Neshaminy Water Resources Authority office at Cross Keys,
Pennsylvania. c. Records <u>Kept at Cross Keys.</u>
MAXIMUM NON-DAMAGING DISCHARGE: Not estimated.

## HEC-1, REVISED FLOOD HYDROGRAPH PACKAGE

The original "Flood Hydrograph Package" (HEC-1), developed by the Hydrologic Engineering Center, Corps of Engineers, has been modified for use under the National Dam Inspection Program. The "Flood Hydrograph Package (HEC-1), Dam Safety Version", hereinafter referred to as, HEC-1, Rev., has been modified to require less detailed input and to include a dam breach analysis. The required input is obtained from the field inspection of a dam, any available design/evaluation data, relatively simple hydraulic calculations, or information from the USGS Quandrangle maps. The input format is flexible in order to reflect any unique characteristics of an individual dam.

HEC-1, Rev. computes a reservoir inflow hydrograph based on individual watershed characteristics such as: area, percentage of impervious surface area, watershed shape, and hydrograph characteristics determined from regional correlation studies by the Corps of Engineers, Baltimore District. The inflow is routed through the reservoir using spillway discharge data obtained from the field inspection or design data. Flood storage capacity is determined from USGS maps or design information and verified by the field inspection. In the event a spillway cannot discharge 0.5 PMF without overtopping and failure of the dam, downstream channel characteristics obtained from the field inspection and USGS maps are inputed and flows are routed downstream to the damage center and a dam breach analysis is performed.

Included in this Appendix are the HEC-1, Rev. pertinent input values and a summary print-out tables.

## Railroad Creek Dam Hydrology/Hydraulics

Classification (Ref. - Recommended Guidelines for Safety Inspection of Dams)

- 1. The hazard potential is rated as "High" as there would be loss of life if the dam failed.
- 2. The size classification is "Intermediate" based 1610 Acre-Feet total storage capacity.
- 3. The spillway design flood, based on size and hazard classification, is the Probable Maximum Flood (PMF).

Hydrologic/Hydraulic Analysis

The complete H & H design folder was available for review. The PMF inflow hydrograph was determined according to procedures in the SCS National Engineering Handbook, Section 4 (NEH-4). The routing was done according to procedures in NEH-5 (not available for review) and, later, checked by SCS computer program, TE-20. The computer routing indicated a higher maximum water elevation than the original flood routing. As land rights were obtained before the computer routing, it was decided to lower the emergency spillway elevation and retain the original flood routing as basis of design. It was decided to evaluate the spillway adequacy using the HEC-1, Dam Safety Version, computer program.

Original design parameters were checked against current information and/or criteria. The drainage area of 3.39 square miles is verified by current USGS maps.

Calculations for the PMF inflow hydrograph were based on a 6-hour rainfall of 25.5 inches and a Runoff Curve Number of 80. Rainfall criteria established for this investigation by the Corps of Engineers indicate a 26.6 inch rainfall (Pef. Hydrometerological Report No. 33) and the use of Hop Brook Factor, a point rainfall reduction factor. For a watershed of this size, the point rainfall

## Sheet 4 of 12

is reduced by 20%, to 21.1 inches. Thus, the design rainfall is conservative compared to Corps of Engineers criteria. The Runoff Curve Number 80 (CN 80) is based on the hydrologic soil group classification and expected future land use within the watershed. The future land use was based on projections of the Bucks and Montgomery Planning Commission to year 2010. Projected land use includes farm/open, 15.15%; wooded, 12.5%; and residential, 72%. The estimated current developed areas are less than 10% from the 1973 USGS map. The estimated future conditions are judged adaquate.

The emergency spillway discharge was checked according to current SCS criteria, TR-39. The maximum emergency spillway discharge was estimated as 15,000 cfs (see sheet 5), about the same as emergency spillway discharge used in the SCS computer routing. The maximum capacity of the reservoir used in the computer routing was somewhat less than the value from the calculations in the design folder. The capacity values reported are less than the actual values as the borrow sources were from within the reservoir area.

Snyder's hydrograph parameters, tp and cp, shown on sheet 5, were used to determine the PMF inflow hydrograph. The peak inflow value is estimated as 10.360 cfs, less than the emergency spillway capacity, therefore, no reservoir routing was required.

The spillway is rated as "Adequate" as the spill-ways will pass the PMF without overtopping the embankment.

Railroad Crack Dam  Hydralagy / Hydrawlics  Emergency Spillmay Capacity ref TE:39  bottom width - 250 H.  louid section - 30.41  total longth - 600 H  approach channel slope - 2.01  assume Q:15 acc cfs   H  depth at supstrain edge of level section - 5.7 H  selectly boad at contained - 1.35 H  selectly boad at contained - 2.19  total head at entrance to approach channel - 1.35 H  selectly boad at contained - 2.19  total head at entrance to approach channel - 1.35 H  selectly boad at entrance to approach channel - 1.35 H  selectly boad at entrance to approach channel - 1.35 H  selectly boad at entrance to approach channel - 1.22 H  total head at entrance to approach channel - 1.22 H  claudion to water death - welency head  -2.24 + 1.35 + 0.19 = 2.23 H t class to  1.2.24 + 1.35 + 0.19 = 2.23 H t class to  Sayder's hydrograph parameters, to feel of the selection of	87	MFB DATE 12/10/79	SUBJECT	SHEET
Hydralogy / Hydramics  Emergency Spillway Capacity ref TP: 39  hottom width = dSD H.  level section = 30 ft  total length = 600 ft  approach channel Slape = 0.01  assume Q = 15 000 cts  g = 0/b = 60 cts/ft  depth at upstraw edge of level section = 5.7 ft.  F5: 158, sh. 1 of 10  depth @ container, to approach channel = 1.35 pt  E-159, sh. 2 af 10  selecity had at entrance = 0.19  fold head at entrance to approach channel =  cleation t water depth to along the selection to 290, 2 ft, meximum  -224, ft + 1.35 t 0.19 = 292, 1 ft alose to 290, 2 ft, meximum  in Q = 15,000 cts  Snyder's hydrograph parameters, to feep  to 2 contain the selection studies by Carps of  Co = 1.50 from correlation studies by Carps of  Co = 0.61 Faguress, Bott Dist, for zone 6  1 = 390 miles from U.S.G.S. map.  Lea = 1.30 miles from U.S.G.S. map.  Lea = 1.50 (2.98 · 1.28)	CHKD. SY	DATE	Railroad Creek Dam	JOS Ne.
Emergency Spillway Capacity ref TP:39  bottom width: 250 H.  level scotton: 30 lt  total length: 600 ft  approach channel slope: 0.01  assume Q:15 000 cts  g:0/b: 60 cts/ft  g toph at apstraw edge of level section: 5.7 ft.  F5:158, sh. 1 of 10.  depth at apstraw edge of level section: 4.7 ft.  F5:158, sh. 2 af 10  telocity had at entrance - 0.19  F5:159, sh. 2 af 10  telocity had at entrance to approach channel:  elevation t water depth t when the Kadi  -274, 4+135 t 0.19 = 282.1 ft. was to  293, 2 ft. was to  293, 3 ft.				
bottom width: 250 H.  land section: 30 ft  total length ~600 ft  approach channel slope: 0.01  assume Q: 15 000 cfs  g: 0/b: 60 cfs/ft  depth at upstrain edge of level section: 5.7 ft.  #3 158 sh. 10 f 10  dapth @ entrance to approach channel - 13.5 ft  E3-158, sh. 2 af 10  velocity hand at entrance ~ 0.19  velocity hand at entrance ~ 0.19  fold head at entrance to approach channel:  elevation + water depth + velocity head  -212, ft + 13,5 ft 2.19 = 292.1 ft alase to  292,2 ft movimum  water elevation  Snyder's hydrograph parameters, tp f cp  tp: C(L-Les)  5-398 miles:  from USGS map.  Lea: h38 miles:  from USGS map.  Lea: h38 miles:		· · · · · · · · · · · · · · · · · · ·		
bottom width: 250 H.  land section: 30 ft  total length ~600 ft  approach channel slope: 0.01  assume Q: 15 000 cfs  g: 0/b: 60 cfs/ft  depth at upstrain edge of level section: 5.7 ft.  #3 158 sh. 10 f 10  dapth @ entrance to approach channel - 13.5 ft  E3-158, sh. 2 af 10  velocity hand at entrance ~ 0.19  velocity hand at entrance ~ 0.19  fold head at entrance to approach channel:  elevation + water depth + velocity head  -212, ft + 13,5 ft 2.19 = 292.1 ft alase to  292,2 ft movimum  water elevation  Snyder's hydrograph parameters, tp f cp  tp: C(L-Les)  5-398 miles:  from USGS map.  Lea: h38 miles:  from USGS map.  Lea: h38 miles:				
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level section: 30 ft  total length ~600 ft  approach channel slope: 0.01  assume 0: 15 000 cts  b: 60 cts/ft  depth at supstrain edge of level section: 5.7 ft.  E5: 158, sh. 10 ft 10  depth @ entrance to approach channel: -13.5 ft.  E5: 158, sh. 20 ft.  selecity head at entrance ~ 0.19  E3-159, sh. 10 ft.  total head at entrance to approach channel:  elevation: t water depth: twolecity head  -278, ft. 13.5 ft. 0.19 = 2921 ft. alaxe to  292, 2 ft. maximum  water elevation  Snyder's hydrograph parameters, to f. ap  (c=1150) from correlation studies by Corps of  Cp=0.81) Engineers, Batt Dist, for zone 6  L=298 mile: from U.S.G.S map.  Lea: 130 mile: 0.33  tp: 1,50 (298:128)				
level section: 30 ft  total length ~600 ft  approach channel slope: 0.01  assume 0: 15 000 cts  b: 60 cts/ft  depth at supstrain edge of level section: 5.7 ft.  E5: 158, sh. 10 ft 10  depth @ entrance to approach channel: -13.5 ft.  E5: 158, sh. 20 ft.  selecity head at entrance ~ 0.19  E3-159, sh. 10 ft.  total head at entrance to approach channel:  elevation: t water depth: twolecity head  -278, ft. 13.5 ft. 0.19 = 2921 ft. alaxe to  292, 2 ft. maximum  water elevation  Snyder's hydrograph parameters, to f. ap  (c=1150) from correlation studies by Corps of  Cp=0.81) Engineers, Batt Dist, for zone 6  L=298 mile: from U.S.G.S map.  Lea: 130 mile: 0.33  tp: 1,50 (298:128)		60	How width = 250 H.	i
depth ~ 6.00 fl  approach channel slope = 0.01  assume Q: 15 and cfs  g: 0/b: 60 cfs/ft  depth at supstrain edge of level section = 5.7 ft.  F5 158 sh. 1 of 10  depth @ entrance to approach channel - 13.5 ft.  E5-159, sh. 2 af 10  selectly head at entrance ~ 0.19  fold head at entrance to approach channel:  clevation + water depth + welectly head  -270, 4+ 13.5 t 0.19 = 292.1ft. alax to 292.2ft. movimum  water elevation  i Q ~ 15,000 ats  Snyder's hydrograph parameters, to Fap  C=150 from correlation studies by Carps of  Ca=150 from correlation studies by Carps of				
assume Q: 15 and cts  assume Q: 15 and cts  g: a/b: Go cts/ft  g: a/b: Go cts/ft  depth at supstrain edge of level section: 5.7 ft  F5-158, sh. 1 of 10  depth @ entrance to approach channel - 13.5 ft  E5-158, sh. 2 af 10  selecity hand at entrance - 0.19  fold head at entrance to approach channel:  clevation + water depth + welocity head  -272, ft + 13,5 t 0.19 = 292, 1 ft alose to  292, 2 ft, movimum  water elevation  :: Q ~ 15 and cts  Snyder's hydrograph parameters, to F cp  tp: Co(t-tex)  From correlation studies by Corps of  Cp: 0.81				
assume 0: 15 000 cts  g=0/b: 60 cts/ft  depth at upstraw edge of level section = 5.7 ft.  E5:158, sh. 1 of 10  depth @ orthonics to approach channel = 1.3.5 ft.  E7:150, sh. 2 of 10  relocity head at entrance = 0.19  total head at entrance to approach channel:  elevation + water depth + welocity head  -274, ft. 13.5 ft. 0.19 = 292.1 ft. wase to  292, 2 ft. morimum  water elevation  : 0 = 15,000 cts  Snyder's hydrograph parameters, to fap  to = C_150 from correlation studies by Corps of  C_2 = 150 from correlation studies by Corps of  C_2 = 0.51 from U.S.S. map.  Lea: 128 miles  from U.S.S. map.				
depth at upstram edge of level section = 5.7 ft.  depth at upstram edge of level section = 5.7 ft.  E3-158 sh. 1 of 10  depth @ ortrance to approach channel - 13.5 ft.  relocity hand at entrance - 0.19  E5-159 sh. 1 of 2  fold head at entrance to approach channel:  elevation + water depth + velocity head  -274 ft   3.5 t   0.19 = 272 lift alase to  292.2 ft, meximum  water elevation.  Snyder's hydrograph parameters, to fap  to = C(L-La) 5.3  from correlation studies by Corps of  Ca=150 from correlation studies by Corps of  Ca=150 from correlation studies by Corps of  L= 298 miles from U.S.G.S map.  La=128 miles from U.S.G.S map.			IPPOREN CHEMIEL STOPE - 0.01	· i
depth at upstram edge of level section = 5.7 ft.  depth at upstram edge of level section = 5.7 ft.  E3-158 sh. 1 of 10  depth @ ortrance to approach channel - 13.5 ft.  relocity hand at entrance - 0.19  E5-159 sh. 1 of 2  fold head at entrance to approach channel:  elevation + water depth + velocity head  -274 ft   3.5 t   0.19 = 272 lift alase to  292.2 ft, meximum  water elevation.  Snyder's hydrograph parameters, to fap  to = C(L-La) 5.3  from correlation studies by Corps of  Ca=150 from correlation studies by Corps of  Ca=150 from correlation studies by Corps of  L= 298 miles from U.S.G.S map.  La=128 miles from U.S.G.S map.	-	4 6 6 7	- A. 15 and Ch	
depth at upstram edge of level section = 5.7 ft.  F5:158, sh. 1 of 10  depth @ entrance to approach channel = 13.5 ft.  E5:158, sh. 2 of 10  relocity head at entrance = 0.19  F5-159, sh. 1 of 2  total head at entrance to approach channel:  elevation + water depth + velocity head  -278, ft + 13.5 t 0.19 = 292.1 ft. clase to  292, 2 ft, more imm  water elevation  O = 15,000 ats  Snyder's hydrograph parameters, to Ecp  to: Co(Like)  F3 from correlation studies by Corps of  Cp=0.81 Faginers, Batt. Dist, for zone 6  L=298 miles from U.S.G.S map.  Lea: 1.50 (2.98.1.20)  1.50 (2.98.1.20)  1.50 (2.98.1.20)		23341	- All Coal III	
death @ entrance to approach channel = 13.5 ft  ES-158, sh. 2 of 10  relocity hoad at entrance = 0.19  fold head at entrance to approach channel:  clevation + water death + velocity head  -218, 4 + 13.5 + 0.19 = 292, 1ft alose to 292, 2ft, mornimum  water elevation  : 0 - 15,000 cts  Snyder's hydrograph parameters, to fap  to = (150) from correlation studies by Corps of  Co = 0.51 Faginers, Bott Dist., for zone 6  L=298 miles from U.S.G.S map.  Lea: 1.20 miles 3		***************************************	= W/D= 60 CFS/ ##	
death @ entrance to approach channel = 13.5 ft  ES-158, sh. 2 of 10  relocity hoad at entrance = 0.19  fold head at entrance to approach channel:  clevation + water death + velocity head  -218, 4 + 13.5 + 0.19 = 292, 1ft alose to 292, 2ft, mornimum  water elevation  : 0 - 15,000 cts  Snyder's hydrograph parameters, to fap  to = (150) from correlation studies by Corps of  Co = 0.51 Faginers, Bott Dist., for zone 6  L=298 miles from U.S.G.S map.  Lea: 1.20 miles 3				1:
depth @ entrance to approach channel = 13.5 ft.  E3-158, sh. 2 af 10  selecity head at entrance = 0.19  E5-159, sh. 1.1 2  total head at entrance to approach channel:  clevation + water depth + velocity head  -218, ft + 13.5 t 0.19 = 222.1 ft. alose to  292, 2 ft, meximum  water elevation  \[ \text{C} \times C_1 (L: Lea)^{\text{D}:3} \]  Snyder's hydrograph parameters, to feep  to = C_2 (L: Lea)^{\text{D}:3}  \text{Trom correlation studies by Corps of Co = 0.81}  \text{Esquirees, Batt. Dist., for sone 6}  \[ \text{L} = 298 \text{ miles} \]  \text{La: 1.30 miles}  \text{Trom U.S.G.S. map.}  \text{La: 1.50 (2.98:1.28)} \]	<del> </del>	4	epin at apstroam edge of level	Section = 5./ ft.
Solution had at entrance - 0.19  Follow had at entrance to approach channel:  Clevation + water depth + velocity head  -278, 4 + 13,5 + 0.19 = 292.1ft. clase to 292,2ft, meximum  water elevation  O - 15,000 ets  Solution:  La 298 mile:  La 298 m			F5.	150, sh. 1 of 10
Snyder's hydrograph parameters, to FCP  Co CL La D' S  Snyder's hydrograph parameters, to FCP  Co CL La D' S  Co Co SI Figure Shift, for some 6  La 298 miles S  Lea = 1,28 miles S  Lea = 1,50 (2.98.1.28)			eath @ Buttance to approach che	annel - 13.5 Ft.
fold head at entrance to approach channel:  Clevation + water depth + velocity head  -278, 4 + 13.5 + 0.19 = 292.1 ft. alase to 292.2 ft. mornimum  water elevation  O ~ 15,000 cts  Snyder's hydrograph parameters, to fap  to fact the standard from correlation studies by Corps of  Co = 150 from correlation studies by Corps of  Co = 0.81 Figures, Balt Dist, for some 6  L=298 miles  to 1,50 (2.98.1.28)  to 1,50 (2.98.1.28)	ļ		<i>F</i> S:	158, sh. 2 at 10
Snyder's hydrograph parameters, to Fap  Compared to the content of		To the second	elocity head at entrance - 0.19	
clevation + water depth + velocity head  -271, ++ 13.5 + 0.19 = 292.1 th. class to  292.2 ft, morning  water elevation  : 0 ~ 15,000 cts  Snyder's hydrograph parameters, to fap  to = C_{\text{L}:Lext} \( \text{L} \)  C_{\text{miles}} \( \text{L} \) from correlation studies by Corps of  C_{\text{p}} = 0.81 \) From Correlation studies by Corps of  L=298 miles \) from U.S.G.S map.  Las: 128 miles \)  to = 1.50(2.98.1.28)	<del>                                     </del>			
-278.4 + 13.5 h 0.19 = 292.1 ft. clase to 292.2 ft. morning water elevation  Q ~ 15,000 cfs  Snyder's hydrograph parameters, to fap  to C(t. Le)  C=1.50 from correlation studies by Corps of C=0.81 Figures, Bat. Dist., for zone 6  L=2.98 miles. from U.S.G. S. map.  Lea: 1.28 miles.	<u></u>	<u> </u>	otal head at entrance to approa	ch channel:
-278.4 + 13.5 h 0.19 = 292.1 ft. clase to 292.2 ft. morning water elevation  Q ~ 15,000 cfs  Snyder's hydrograph parameters, to fap  to C(t. Le)  C=1.50 from correlation studies by Corps of C=0.81 Figures, Bat. Dist., for zone 6  L=2.98 miles. from U.S.G. S. map.  Lea: 1.28 miles.	<u> </u>		elevation + water depth + u	elocity head
Snyder's hydrograph parameters, to Fap  to = (L-La) 5.3  Co = 150 from correlation studies by Corps of  Co = 0.81 From U.S.G. S map.  Lea = 1,28 miles  to = 1,50 (2.98.1.28)			-278, ++ 13,5 + 0.19 =	292 1 ft wase to
Snyder's hydrograph parameters, to FGP  tp: Co (L-Lea) 5.3  Co = 150 from correlation studies by Corps of  Co = 0.81 Figures, Batt Dist., for zona 6  L: 298 miles from U.S.G.S map.  Lea: 128 miles 0.3  tp: 1.50 (2.98.1.28) 0.3	<u> </u>			
Snyder's hydrograph parameters, to FGP  tp: Co (L-Lea) 5.3  Co = 150 from correlation studies by Corps of  Co = 0.81 Figures, Batt Dist., for zona 6  L: 298 miles from U.S.G.S map.  Lea: 128 miles 0.3  tp: 1.50 (2.98.1.28) 0.3	1			water elevation
Snyder's hydrograph parameters, to Fap  tp = C_1(1-1_2) b.3  C_2 = 1/50 } from correlation studies by Corps of  C_2 = 0.81 } Engineers, Batt. Dist., for zone 6  L= 2.98 miles } from U.S.G. S. map.  Lea = 1/28 miles }  tp: 1.50(2.98.1.28)			· 0 ~ 15,000 cts	
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Cp = 0.81			C= = 150 Law correlation	studies by Gros of
L= 298 miles ) from U.S.G. S. map.  Lca = 128 miles )  tp: 1.50(2.98.1.28)				
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tp: 1.50(2.98.1.28) 0.3	<del></del>			1
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		1.	150(2.98.120)0.3	
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12/21/64 JDG

PA 615 NESHAMINY

70+

STAGE STORAGE COMPUTATIONS

(DAM IN PLACE)

1 = 180.79 Ac-ft.

1142=	0.918 Ac							
	AREA	AREA	2 Area	Aug Area	Dist	Vol	CUM	
STAGE	SaIn	Ac	Hc	Ac	FT	ACFT	AcFT	
							_	
258	0						0	
<b></b>			0.86	0.43				
260	0.94	0.86						
			8.66	4.33	5	<u> </u>		
265	8.52	7.8	<u> </u>	13.5	5		2.3	
<u></u>			26.7	13.35	- <del>3</del>	67		-
270	20.54	18.9		_			90-	7 7 <sup>7</sup> 4 .
	<u> </u>		53.5	26.75	5	13.4		
275	37.70	34.6	<del> </del>				224	:/ <u>:</u>
			92.2	46.1	5	23)	1 -1=	
280	62.69	57.6	1111		<u></u>		455	<u> </u>
			146.4	73.2	5	366	<b>1</b>	
285	96.63	88.5	- 1-0	1000			821	77.6
-	<del> </del>		217.8	108.9	5	545		
290	140.17	129.0		. 4 -		741	1366	3355
			2984	149.2	5	746		
295	184.43	169.4	1 -				2/12	* 2 -
	£.V01			Eff Vol Inches			<del>                                     </del>	
Elev	inahre	1	Elev		Ac: Fr.	<u> </u>	<del> </del> -	
259	-	<del> </del>	267.5	-	0_	-	+	
260	0.006		270	0.20	36.2	:	+	
265	0,/3	<del> </del>	275	0.89		<del> </del>	1 1 1 10	
270	0.50	<del> </del>	290		392.3	26	11-1 ky 15	2-/2-7
2.75	1.24	<del> </del>	285	1	757.5	<del>                                     </del>	1	1
. 580	2.52	<b></b>	290	T	1310.7		REF:- SCS DESIGN	
285	7.55	<del> </del>	295	11. 33	2043.4	-	FOLDER	
295	11.68		1	1	1,	<u>L</u>		1

SHAMINY	MESHAMINY CREEK PA-61	<b>S</b>			JHF 11-72
	CURVE NO.	60. TC	1.53	STORM DURATION	9.00
E	MER. SPW. RA	EMER. SPW. RAINFALL 10.50	FREESOA	FREESOARD RAINFALL 25.50	• 50
CASE NO.	÷	DRAINAGE AREA	A 3.39	EMER. SPW. CREST	REST 285.0
109	5C. L1	500. 602	• L2 0•	803 0· L3	•0
	ELEVATION	STORAGE	CFS	CFS CF	S
:	285.00	821.	107.	0.	•
	287.00		2482.	.0	
	289.00	. •	4857.	•	•
	289.26		5165.	0.0	
	250:29	· -•	7617.	0.0	•
	251.00	i	9724.	0.	
•	292.33	•	13671.	0.0	•
-	293.00	-	15098.	0.0	
	254.36		21025. 1.	0.	•
	254.59	· . · ·	23716.	0	
			-		
:	:				REF: -
					SCS DESIGN
:					FOLDER

Company of the second		46															••			endebende tre destructions of the contract of the country of the contract of t										S#	10/81 - AFCEJ = 16,21				
FREEBOAKD AQUITING	1.1 JHF 11-72						•	***************************************		292.51 1705.67 Tea of D.	PEAK OCCURS PREVIOUS LINE									REF:	SCS DESIGN	FOLDER						The profession of the case of		AT HP IS 0.15 PERCENT. 7.87 FLOW THRU EMERGENCY SPILLMAY - 10.79 H	C SPILLWAY PER FOOT OF MOLTON MIGHN SO/BL				
	-	205.00			205.15		J		ł	292.57	292.74	292-42	291.59	290.77	290.42	289.69			268.82		287-53	,	~ ^		285.61			•	285.09	VOLUME CHECK AT COMPUTED HP 7. DLKATION HF FLOX	IAU THE ENENGENCY			i	
1			OBTFLO	107.	293	926.	1579.	4301.	7420	1957	15190	2750	1480	9636	9632	6677	6143	5C56	4649	3636	3123	222C.	1847	1252.	633	5	7,7	35.	**		-		:	1	-
		O. CAEST	AVE IN	161.	912.	2403.	4159.	10756.	14692.	17856.	14765.	11254.	9858	7553.	6731.	5670.	5227	3895.	3038.	1582.	1107.	537.	370.	172.	120	50.	31.	•	90		VOLUME OF OUTFLOW			-	
	EEK PA-615	1 - 500.	INFLOW	215.	1001	3095.	5223.	12877.	16507.	1576	13751.	10519.	9196	7083.	6380.	5465	4990	3472.	2603.	1304	911.	439.	301.	139.	61:	39.	12.				YOUNE	:	٠		
	SHAMINY CREEK PA-615	→1 = 250.	1186	1.00	1.50	2.00	2.25	2.75	3.00	3.50	00.	4.50	5.75	5.25	2.50	4.00	52.9	6.75	7.00	7.50	7.75 M. 60	D.25	8.30 8.35	9.00	9.50	9.75	10.00	10.50	11.00	1 .	PAUSE				

Date - Checked By Date Job No. BY H. L.W. JOB NO. PA-Suoject WORK PLAN - DESIGN COMPARISON Sheet 1 of SHEET 9 OF 12 UNIT WORK PLAN DESIGN ITEM CCMMENTS DRAINAGE AREA 3.37 SQ. Mt. 3.37 STORAGE CAPACITY SEDIMENT (INC. AERATED) AC FT BENEFICIAL ACFT 722 714.1 RETARDING :. AC FT. TOTAL 795 AC FT BETWEEN HIGH & LOW S. ACFT. SURFACE AREA NORMAL POOL ACRE 13 RETARDING POOL 36 85 ACRE DESIGN HIGH WATER ACRE 110 71,000 VOLUME OF FILL CU YO. 291.7 272.2 TOP OF DAM ELEV FEET 34.7 MAX. HEIGHT OF DAM FEET EMERGENCY SPILLWAY CREST ELEVATION 284.6 784.5 FEET 730 BOTTOM WIDTH FEET TYPE 50d 304 PERCENT CHANCE OF USE <u>--</u>--280 30 AVE CURVE NO COND II EM. SP HYDROGRAPH ∠\_ 2 74.5 10.5 STORM RAINFALL - 6 HR. IN. 8.0 STORM RUNGEF IN. 3.0 ·7. X VELOCITY OF FLOW - V FPS 7.2 2,200 2288 PEAK DISCHARGE RATE CFS 2 37.1 287.5 MAX WATER SURFACE EL FEET FREEBOARD HYDROGRAPH 25.5 25.5 . STORM RAINFALL - 6 HR. IN. STORM RUNOFF IN 22.73 22.73 FPS 13.1 14.7 VELOCITY OF FLOW - V CFS 13,12 5 PEAK DISCHARGE RATE 13,45% 27/.7 2 7 Z. Z. MAX. WATER SURFACE EL. FEET PRINCIPAL SPILLWAY 24x74 RISER SIZE FT 113.9 106 MAX. LOW STAGE FLOW CFS ORIFICE SIZE FT. SCS DESIGN MAX: HIGH STAGE FLOW CFS FOLDER PIPE SIZE DIA. CAPACITY EQUIVALENTS TOTAL SEDIMENT VOL. 0.31 1 N 3.95 3.77 RETARDING STORAGE IN EM. SPILLWAY STORAGE TO TOP OF DAM IN. CLASS OF STRUCTURE CONSTRUCTION COSTS S-C RATIO

wp-0C-1

JULY 1978 DAN SAFETY VERSION
JULY 197
LAST MODIFICATION 25 FEB 79

RUN BATE\* 79/12/10. TIME\* 14.18.14.

RAILROAD CREEK DAN BER NO. 9-175 INFLOW HYDROGRAPH

	IFRY	- 4		
	IPL	<b>-</b>		
2	THR ININ HETRE	0	TRACE	0
IFICATIO	NIUI	•	LROPT	0
JUB SPEC	INR.	•	במא	0
	IDAY		JUPEK	L')
	2 .	2		
	Z C	>		

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MILTI-PLAN ANALYSES TO BE PERFURMED NPLAN= 1 NRTIO= 1 LRTIO= 1

1.00 R7105=

B JWB3

5807

EXES

Ke JR

NO.DA HR.AN PERIOD

END-OF-PERTOD FLOU COMP 0 NO.8

1088

EXCS

RAIM

MO. BA HR. MM FERTUD

26.88 24.47 2.42 2132/3. ( 683.) ( 621.) ( 61.) ( 6059.22)

RUS

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# SUB-AKEA KUNOFF CONFUTALION

INFLOW HYDROUSRAPH

						291.
01041	4°		871MP 0.00			VOL: 1.00 803. 119. 10.
INANE ISTAGE	IE LOCAL I 0		AL SMX 0.00			
INANE	J ISAME	696 0.00	CNSTL ,		00	CF= .8 780. 153.
JPRT 0	0 MONST	R72	STRTL CI	•	RTIOR= 2.00	2.22 HOURS, CP= .80 717. 780. 195. 153. 17. 13.
JPL I 0	KATIU 0.000	K48	KTIOK ST 1.00 1	ΙΑΞ		
ITAPE 0	PH DATA TRSPC 0.00	DATA R24 132.00		КОБКАРИ <b>D</b> 6 CP= .81	ON DATA =05	ES, 1.46°
IECON II	HYDROGRAPH DATA TRSDA TRSPC 3.39 0.00	PRECIP DATA R12 R24 123.00 132.00	LOSS BATA N STRKS 0 0.00	HYD	RECESSION DATA ORUSH=(	ORBINAT 493. 318. 28.
ICOMP IE 0	H SNAP 0.00	R6	EKAIN 0.00	UNIT TP= 2.24	-1.50	-PERIOD 367. 406. 35.
	TAREA 3.39	. 50 . 50	KT10L	_	STRT0=	UNIT HYDKUGKAPH 29 END-OF-PERIOD ORDINATES, LAG: 124. 249. 493. 615. 494. 318. 249. 57. 45. 35. 28. 22
ISTAB	1UHG 1	-	PL 1KR 0.00		G	9KAPH 29
	14706	PRUGRAN	STRKR 0.00			1 HYBKG 124. 646. 57.
	-	BY THE	LROP!			UNI 34. 744. 73.
		SPFE 0.00 Inspc computed by the program is				
		IKSFC CI				

PEAK FLOU AND STORAGE (END UF PERIOD) SUMMARY FOR MULTIPLE PLAN-KATIU ECONOMIC COMPUTATIONS FLOUS IN CUBIC FEET PER SECOND (CUBIC NETERS PER SECOND) AKEA IN SQUARE MILES (SQUARE KILOMETERS)

KATIOS APPLIED TO FLUUS

1.00 PLAN RATIO 1 AREA STATION OFERATION

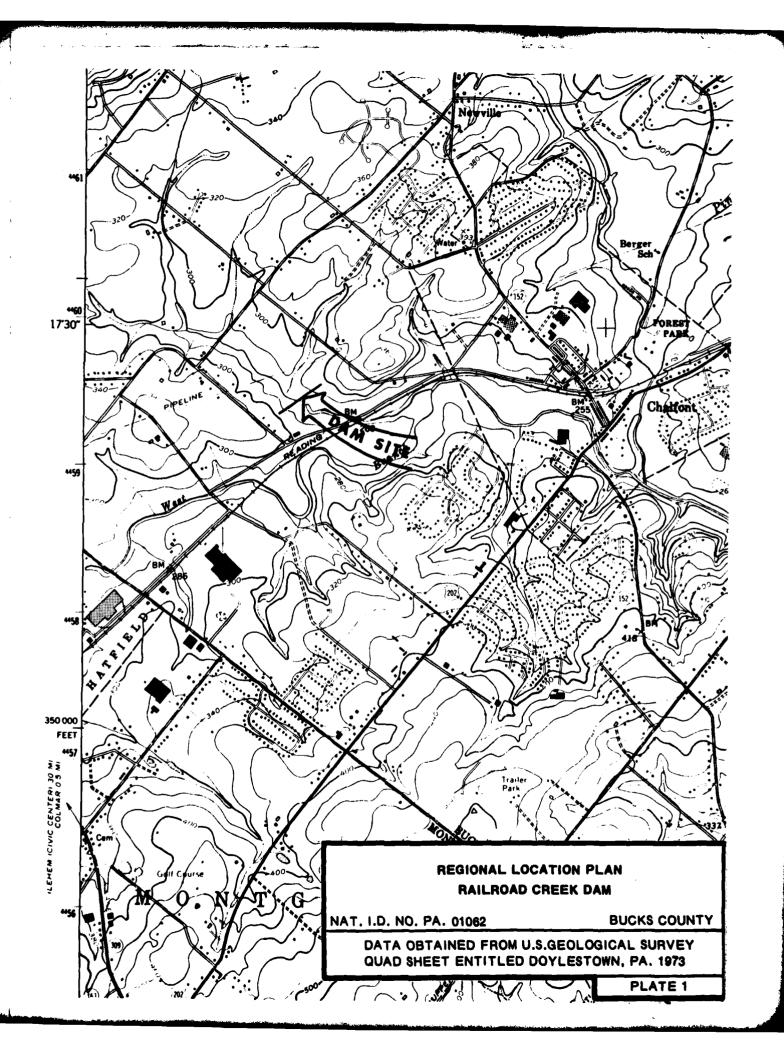
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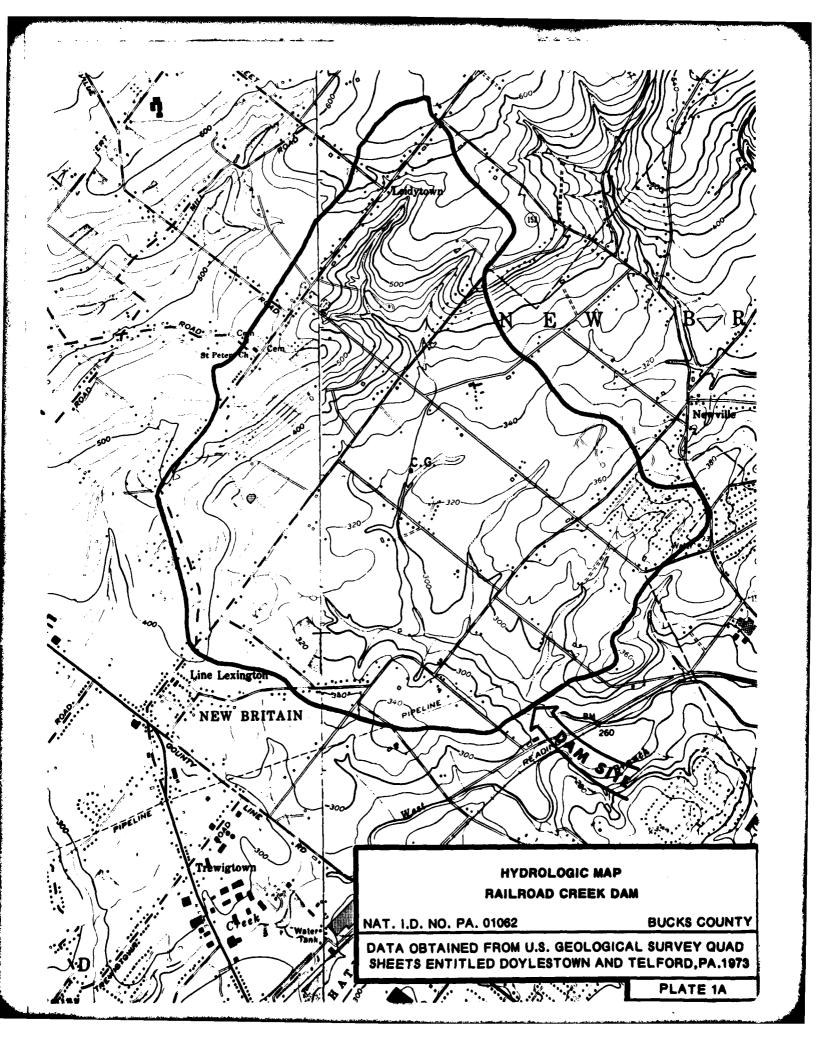
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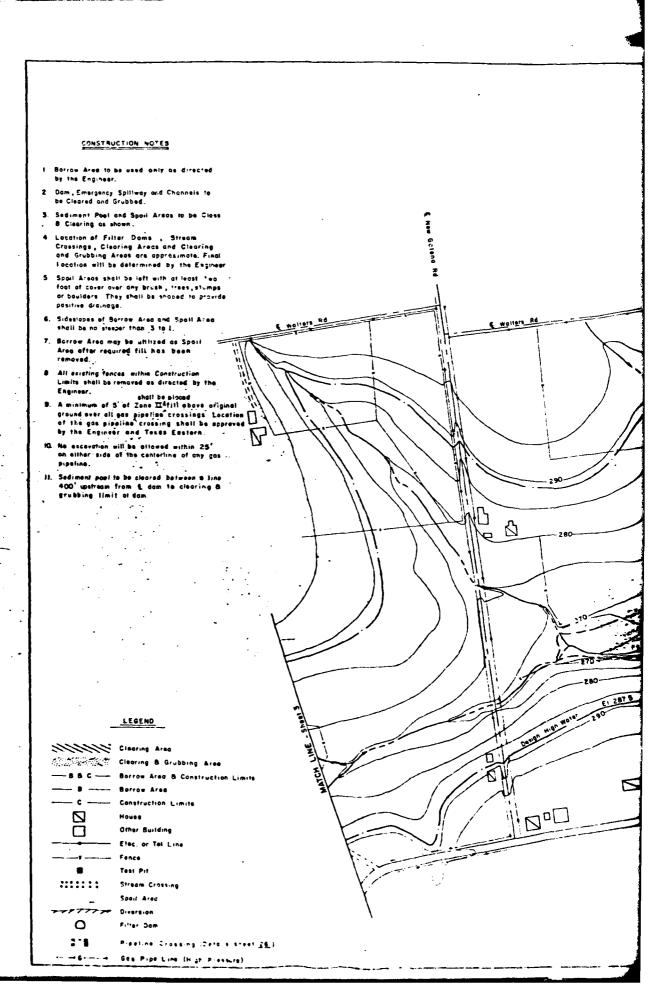
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APPENDIX

E







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Ingress & Egress / (20' Right of Way) TP-105 D BM - 3 SIG 25+00 ٥  $\square$ 0 50 100 200 SCALE IN FEET NESHAMINY CREEK WATERSHED FLODEWATER RETARDING DAM PA - 615 BUCKS COUNTY, PENNSYLVANIA PLAN OF STORAGE AREA U. S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE 4.75

NOT TO SCALE  $_{B}^{H}$ Phila Elec Pole no 95691 Nail head 5' above ground. BM - 5 Sta 6 + 83 Ei 314 3 264\*-07 Phila. Elec Pale no 95690 Nail head 6' above ground 14+07.84 Noil head on 26" Ash tree. Ref ; Apex of Walter Lapp<sup>4</sup> bern Ref 2 Nail head on 6" Wainut 18" above ground. 8W-3 510 25+00 E: 292 40 BW 2 Bress pin of edge of hedge row

Design High Woter El 287.5 
 SW
 RADIUS
 POINT
 LOCATION

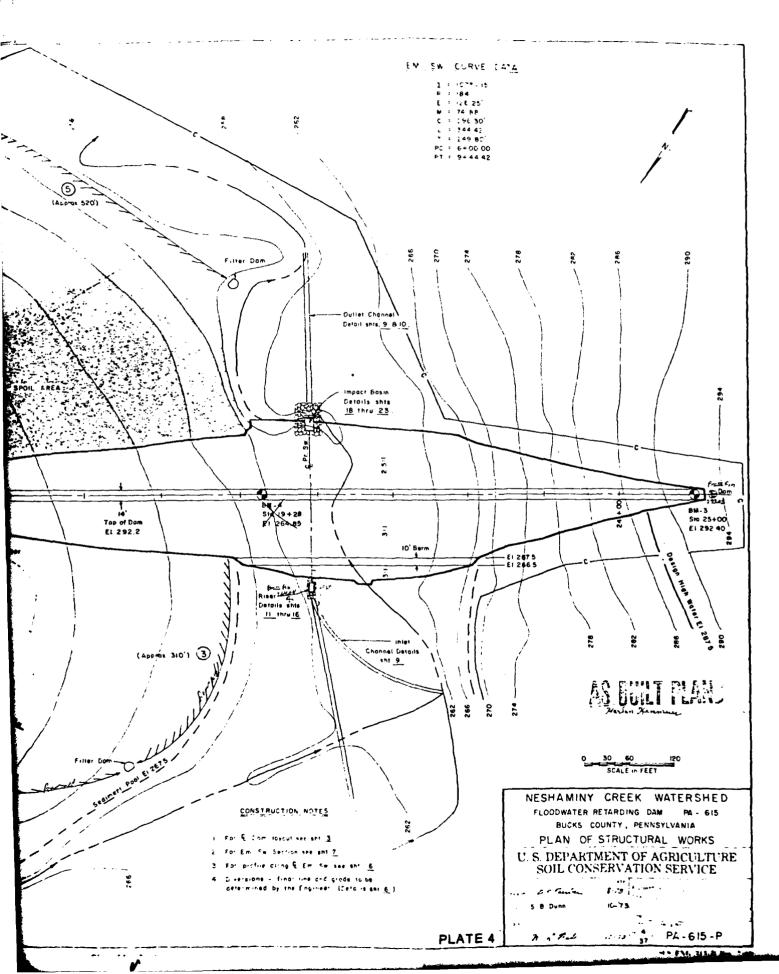
 0 2 5 10 20
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 SCALE in FEET
 AC DULT PLANS 0 50 100 200 SCALE IN FEET NESHAMINY CREEK WATERSHED FLOODWATER RETARDING DAM PA - 615 BUCKS COUNTY, PENNSYLVANIA PLAN OF STORAGE AREA U. S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE . S B Dunn PA - 615 - P

PLATE 3

W - 1 N 4 1 No.

ar ar sin



Stripping Line or Found Esco. Line

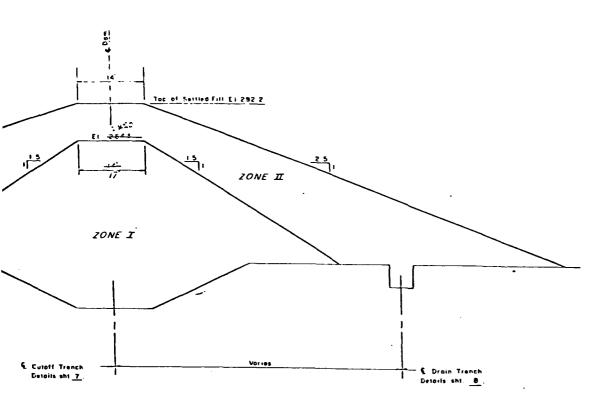
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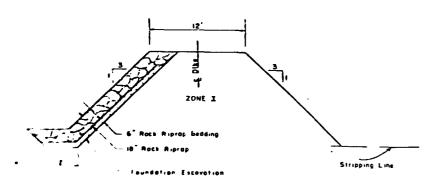
		MAX.	MAX.	REO'D LZ	COMPACTION	
ZONE	MATERIAL	SIZE	LIFT	CONTENT	CL ASS	DEFINITION
1,	Motorial as represented by TP-108.1, depth 0.6' to 4', CL; by TP-216.1, depth 1.7' to 6', CL; by TP-217.1, depth 1'103', ML	•	••	Optimum to + 3 % (	^	95% max density by ASTM, D-698, Method A
л	Motoriol as represented by TP-108.2, depth 4'to 6', 6M; by TP-217.2 B.3, depth 3'to 12.8', GM-GP.	12	18"	Optimum 10 + 3 % (mmus no. 4 moterial)	c	Min 6 passes with 450 psi tamping ratter per lift

Bottom Em Sa

- U Max permissible lift thickness before compaction
- \$2 Water centent of fill matrix at time of compaction. Varation from outer content shown may be approved by the Engineer.
- 3 For typical composition curves see shts. 36 B 37 .
- f for hand compacted backfull the maximum rock size shall not second 3" and lift thickness shall not exceed 4".







# P / AL MOCK RIPRAP SECTION OF DIKE

AS EULT PLAN

### CONSTRUCTION NOTES

1 Constructed slopes are

2.93 | Upstroom 2.46 | Downstroom

2 For constructed fill elevations

see shi 7

NESHAMINY CREEK WATERSHED FLOODWATER RETARDING DAM PA - 615

BUCKS COUNTY, PENNSYLVANIA
FILL PLACEMENT

U. S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE

11.1. Of Contra 8.79

S & Dunn

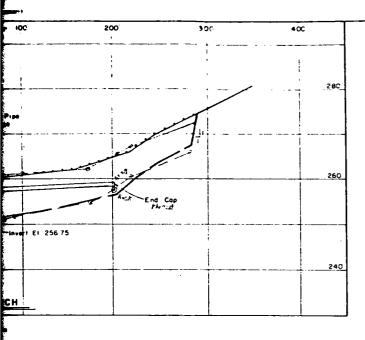
10-71 ....

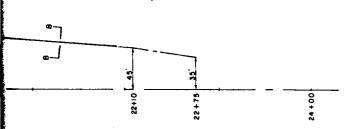
PLATE 5

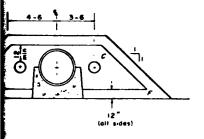
25 PA - 615 - P

1 1 1 h 21 . 1 h . . .

22-00 24 + 00 26-00 4 100 400 600 20 + 00 21+00 11.50 GM SiS ş°'ş Arg or SIS 5,5 Arg ] sis Approx bottom of Cutoff Trench PROFILE ALONG & CUTOFF TRENCH AS BUILT FLANE Toe of Dam (Approx) CONSTRUCTION NOTES 23+30 NESHAMINY CREEK WATERSHED 1 & Dom : & Cutoff Trench FLOODWATER RETARDING DAM 2 For logs of test hores see shts 28 thru 35 BUCKS COUNTY, PENNSYLVANIA PROFILE ALONG & DAM U. S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE ... 10 Carrier 5 E Cunt 9-73 A Bak P4 - 615 - P PLATE 6







SECTION C-C

CONSTRUCTION NOTE

i All 12" drain pipe will be Class For II, Shape 1, Coating A. 6 Sage Perforated (Suec 55),

2 See ant that 12 SMP telanic arrors impair bosin fan. Medal Tiding at American Massie, 2

GRADATION LIMITS

100 to 16 16 1.

FINE CRAIN FILL (F)

SEVE NO NORY WEIGHT:

3/6" 12- 100

10 4 57:2/ 90 - 100

10 10 8 27:79 70 - 100

10 10 8 27:79 50 - 85

10 10 2.60 1 - 8

10 10 2.60 1 - 8

10 200 - 3

werners west Side Plad

CSARSE	4	2.9.6	/A	FI	11	1	c.	,
1.	٠ <u>.                                    </u>	24	55	1945		36	F	r

28	SIEVE NO	% PASSING BASED ON DRY WEIGHT)
٤	1-1/2"	100
ō	<u></u>	34.5 90 - 100
PennDO	1/2"	26 0 - 10
ā	no \varTheta	220 0 - 5
	no 500	- 3

Tested on Site 3-23-77 Fine 4 Course Drain All By Remorar

Man Store Ldong

### DRAIN PIPE QUANTITY SUMMARY

316' - 12" Drain Pipe

2 - I'x I' Elbows, 90°

2 - 1'x 2' Elbows, 90°

2 - 1' £ 2'-4" Elbows, 90°

2 - 1'-6" x 3' Elbows, 90"

2 - End Cops

2 - Small Animal Guards (snt 26)

341'-8" - Total

AS DULL PLATE

NOT TO SCALE

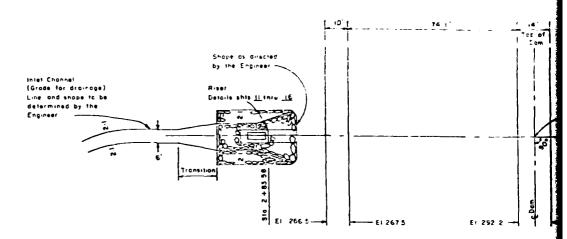
NESHAMINY CREEK WATERSHED
FLOODWATER RETARDING DAM PA - 615
BUCKS COUNTY, PENNSYLVANIA
DRAINAGE

U. S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE

1993 1994 - 1994 1994 - 1995

PLATE 7

1.2 1 11 11/1 11/1 11/2-F

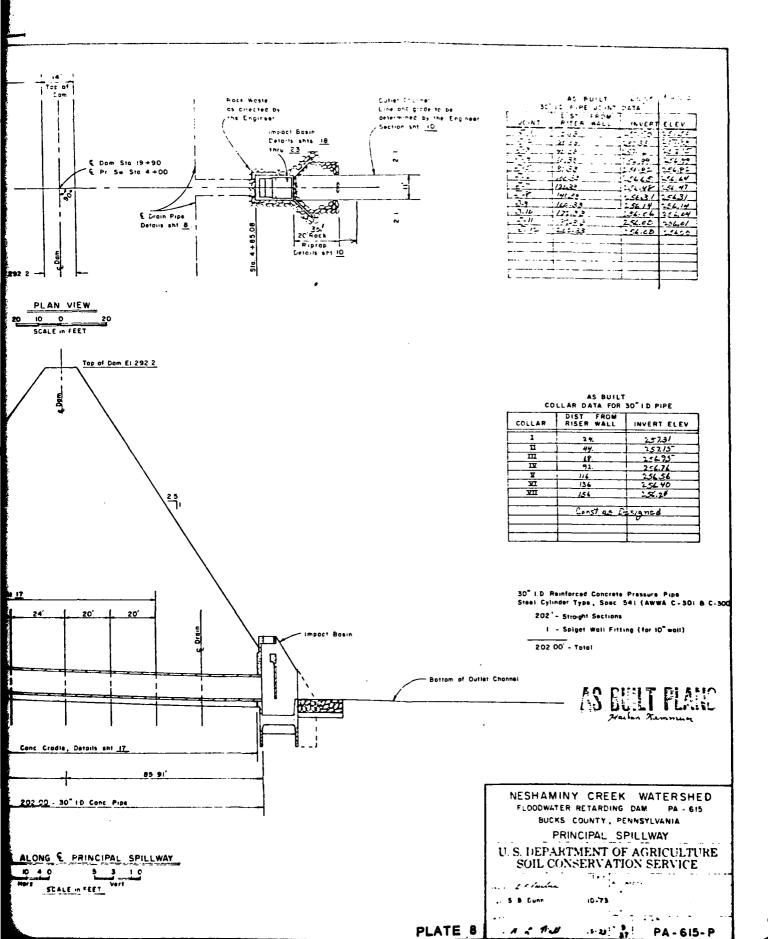


PLAN VIE CONSTRUCTION NOTES 10 0 1. Outlet end of one stondard  $30^{\circ}$  section to be finished so that no metal SCALE IN FEE is exposed and shall be installed at the impact basis. 2. Pipe layout data to be furnished by the Engineer. 3. Riprap bedding shall meet grodation limits for fine drain filt. (sht. 8) 4 For excavation details, see sht 10. 18" Rock Riprop & 6" bedding cover required ground Pipe Ant: - Seep Collers . Details sht 17 Bottom of injet Channel-图 Conc Credie, D 116 42

•

PROFILE ALONG & P

202 00 - 30" (

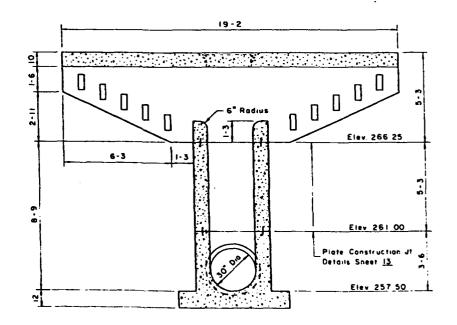


4+00 E + DC . E. Principa Spiriety Stations 300 - Top of Dom, Et 292 2 mpact Basin Original Ground 20' Rock Riprop Section Outlet Channel 7 Fine Draw -Approx Rock Line AS BULL PLANE LONG & PRINCIPAL SPILLWAY Original Ground al state INLET CHANNEL 10' Rock Riprap Section NESHAMINY CREEK WATERSHED FLOODWATER RETARDING DAM PA - 615 BUCKS COUNTY, PENNSYLVANIA PRINCIPAL SPILLWAY EXCAVATION U. S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE OUTLET CHANNEL (Line and grade to be determined by the Engineer)

7-6 10 2-6 10 7-6

Manhale Assembly, Defails Sheet 15

PLAN-TOP



SECTION A-A

High Stage Tree Details Sheet

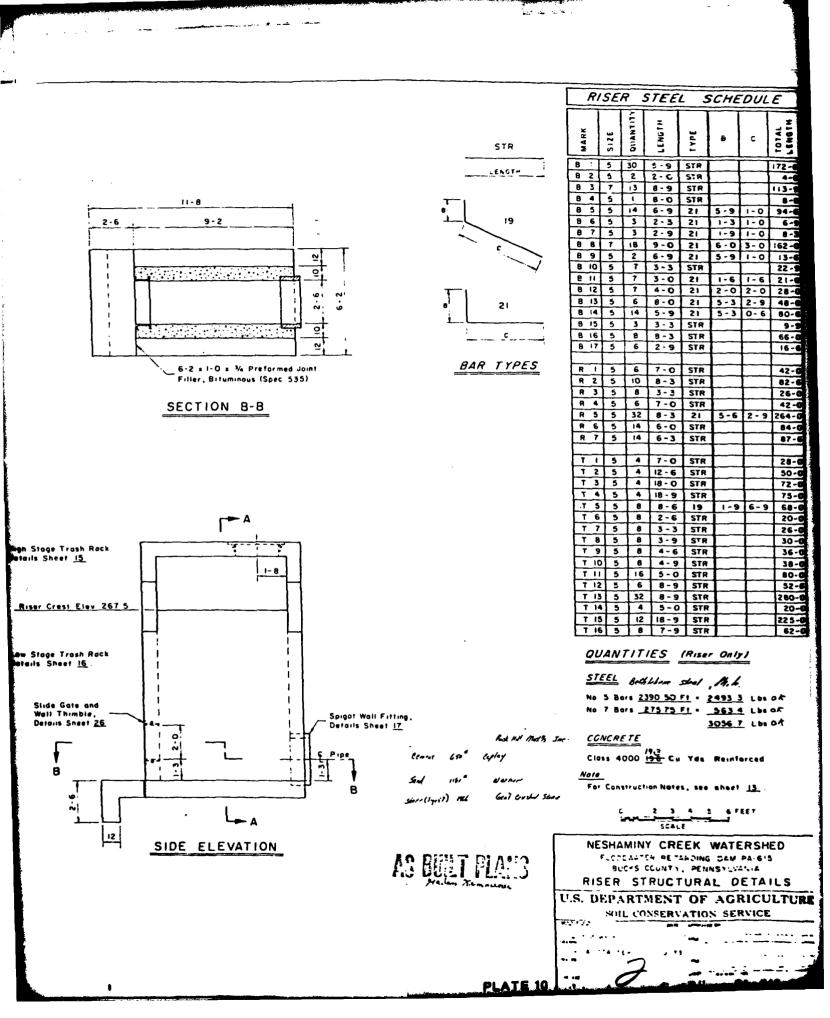
Riser Crest

Low Stage Tres Details Sheet

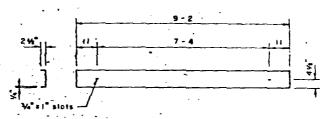
> Slide Gate Wall This Details Sm

F B

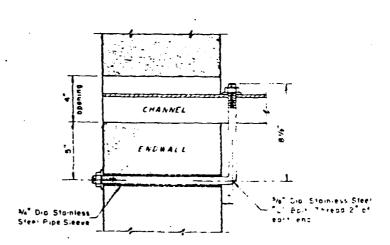
5.8



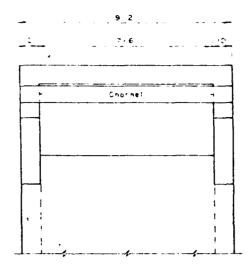
# ENDWALL ELEVATION



# CHANNEL



"L" BOLT DETAIL
SUPPLY A TH MEY NUTS AND
FLAT ADDRESS ASTN, A-276
(STAINLESS STEEL)



# SIDEWALL ELEVATION

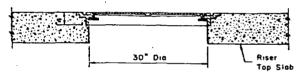
SIZE	LENGTH	QUANTITY
1/2" × 9"	9' - 2"	12
3/4" Dia	0,-10,,	24
3/6" Dio	8 1/2" = 12"	24
	Va" Dia	Va Dia 0,-10,,

R4H Medal Fabricators 3465 Hagareth W. Losson , Fo.

### CONSTRUCTION NOTES

- Channel in trash rack shall conform to Spec 581 for aluminum alloy
- 2 Aluminum surfaces to be placed in contact of an alkali-resistant, bituminous paint before installation

Neenah 5900 - H



### MANHOLE ASSEMBLY

- l. The assembly shall be grey iron casting, class 30, with a  $50^{\circ}$  opening.
- The lifting device shall consist of a l<sup>n</sup> dia hole approx.
   3<sup>n</sup> from the outside perimeter of the lid.
- The locking device shall consist of two rotating bars with hex bolts located under apposite edges of IId.
- 4 Point in accordance with point system A. (Spec B2) Mc Chary , Ph. L.

NESHAMINY CREEK WATERSHED

FLOODWATER RETARDING DAM PA-615 BUCKS COUNTY, PENNSYLVANIA RISER ACCESSORIES

U.S. DEPARTMENT OF AGRICULTURE

SOIL CONSERVATION SERVICE 24 1 ATT ATT 81

C. F. Faceban 4 4 5\*4,\*16

PLATE 11. 7. 2. T.W

PA-615-P

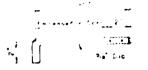
HIGH STAGE TRASH RACK



All points of contact between angles to be welded

CONSTRUCTION DETAILS

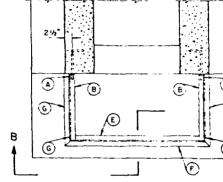
- All angles in trash rack shall conform to Spec 581 for aluminum allay.
- Aluminum surfaces placed against concrete surfaces, shall be given a heavy coat of an alkali-resistant paint before installation.



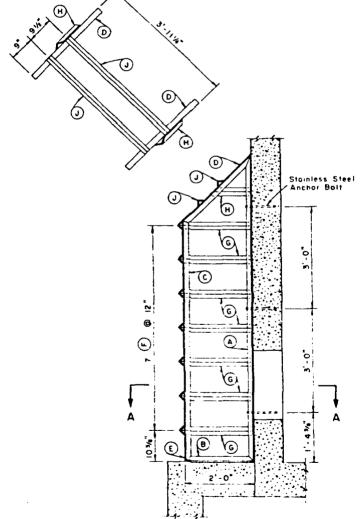
ANCHOR BOLT SUPPLY WITH HEX NUT AND FLAT WASHER, ASTM A- 276 ISTAINLESS STEEL)



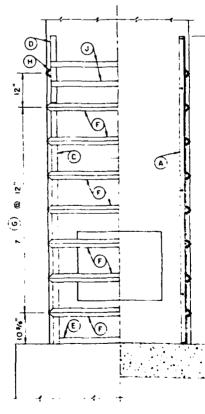
WELDING DETAILS



SECTION A-A

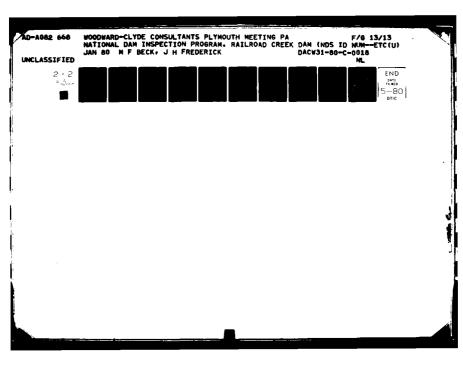


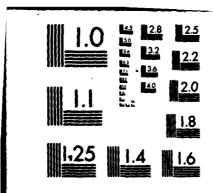
SECTION ON &



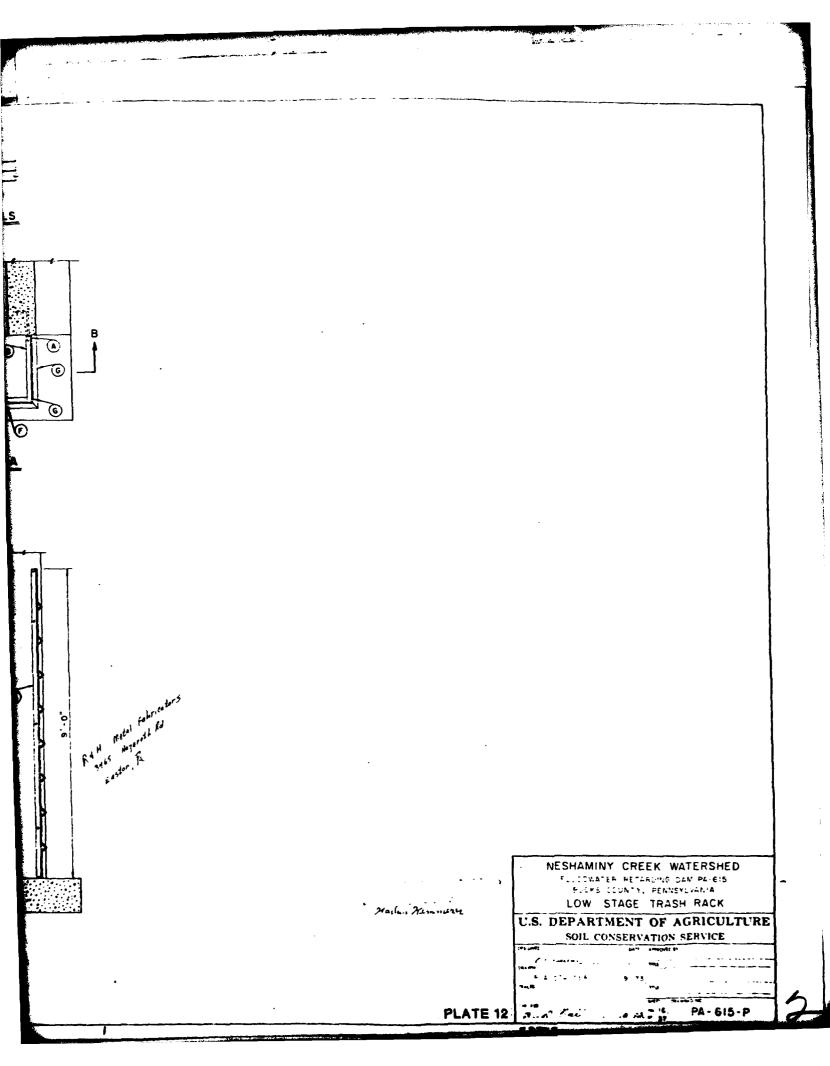
SECTION B.B

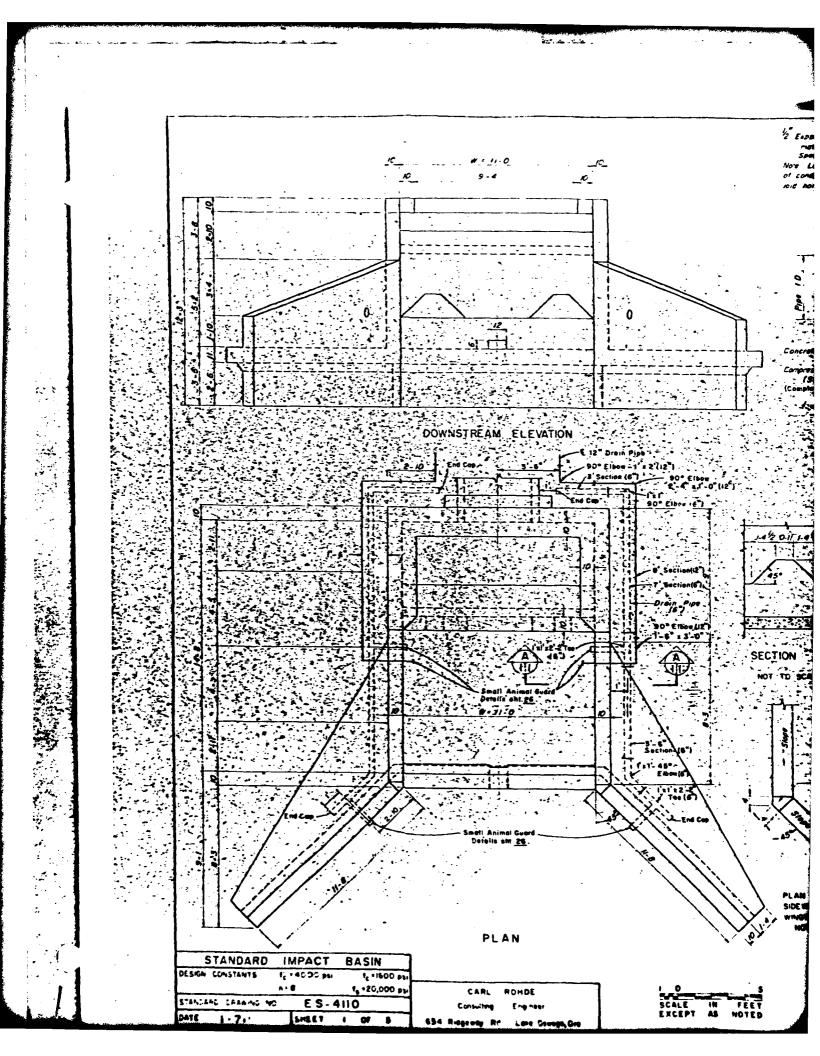
LOW STAGE TRASH RACK DETAILS

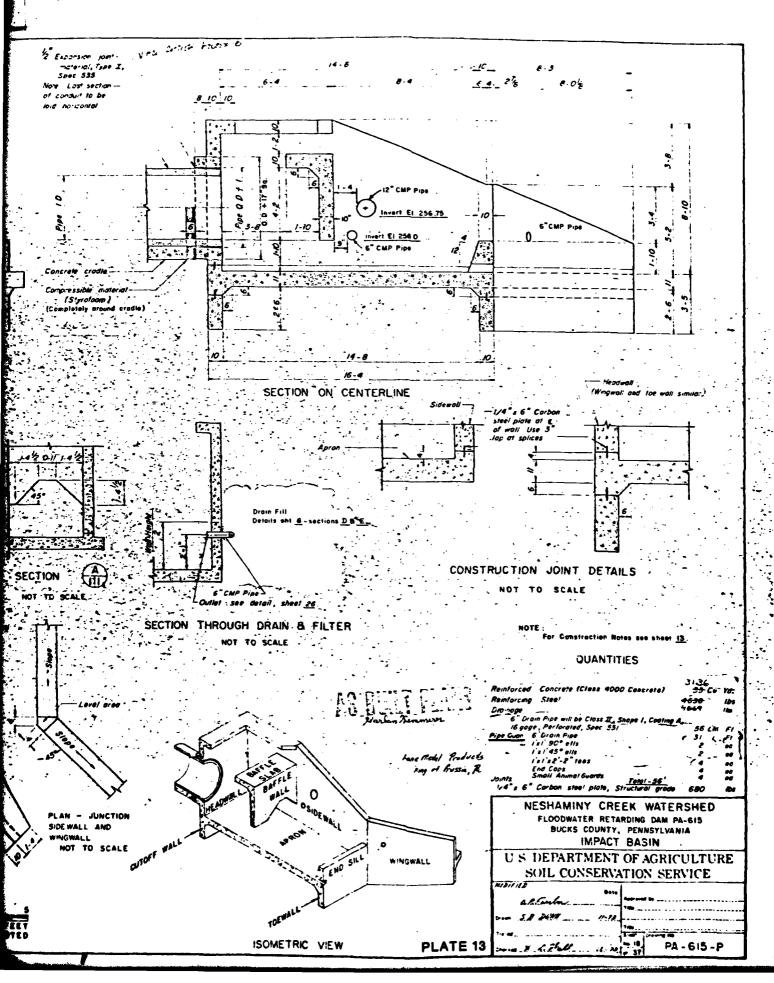


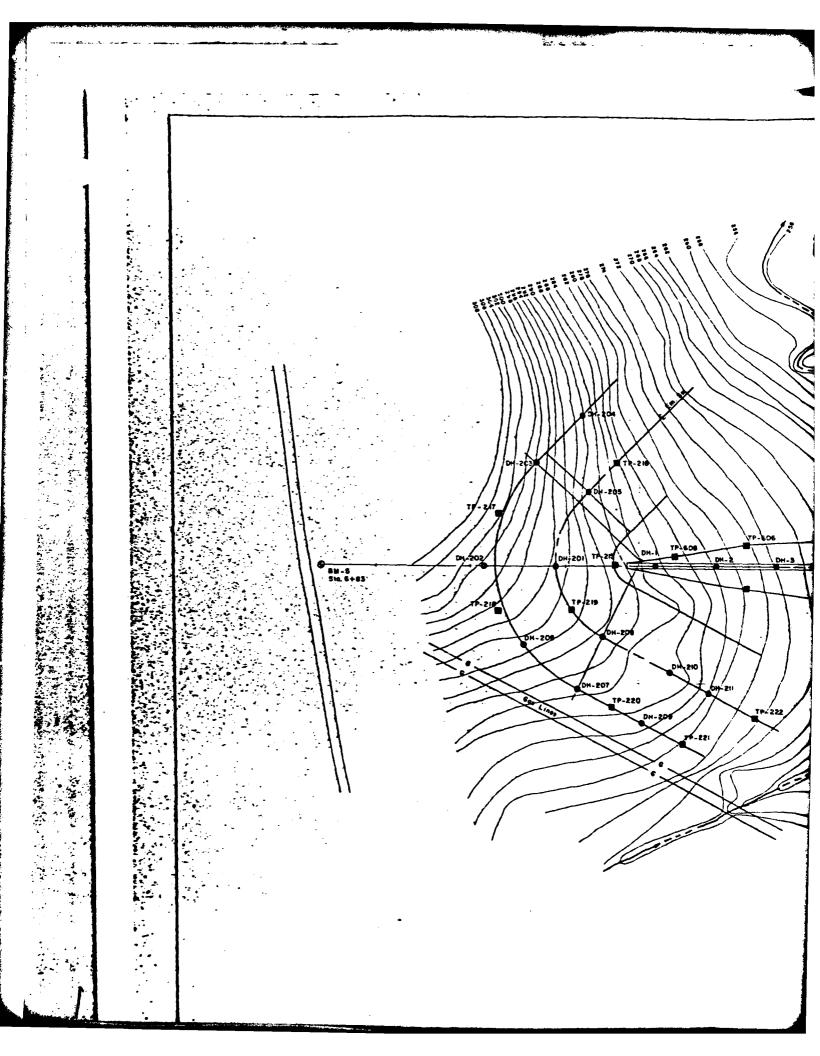


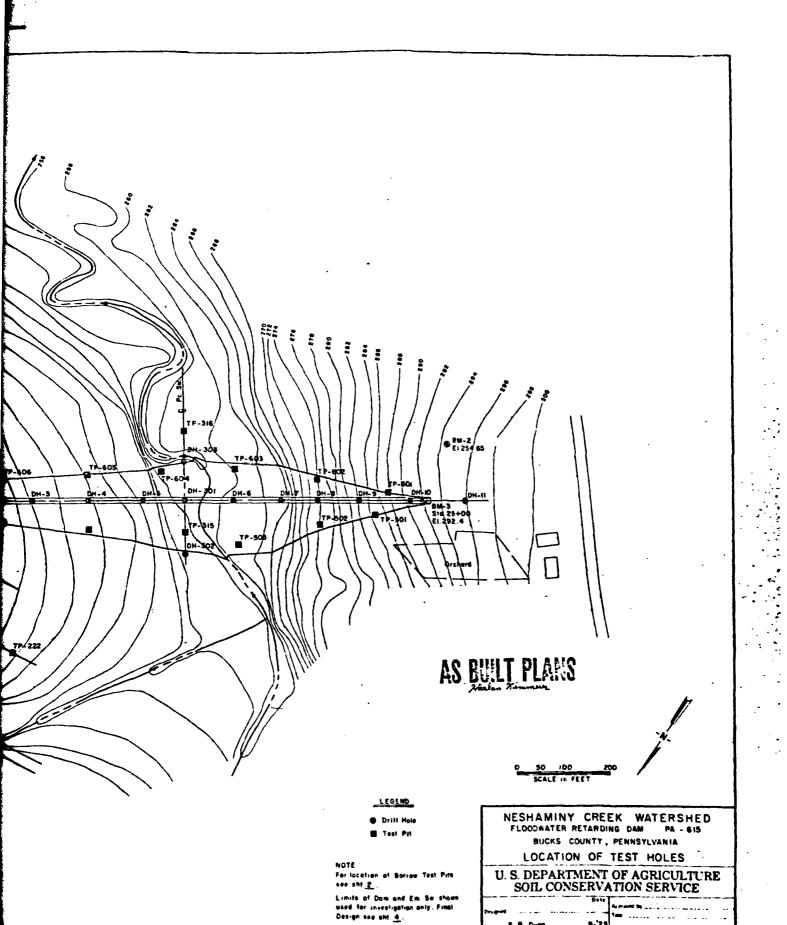
MICROCOPY RESOLUTION TEST CHART











## LEGEND

# TEST HOLE NUMBERING SYSTEM

Centers he of Dam	1 - 99
Borrow area	101 - 199
Emergency spiliway	201 - 299
Centerline of outlet structure	301 - 399
Stream channel	401 - 499
Relief wells	501 - 599
	601 - 699
	701 - 799

•	GW	Well graded gravels, gravel-sand mixtures
٠.	GP .	Poorly graded gravels
;	GM-	Sitty gravels, gravel-sond-sitt mixtures
	GC .	Clayey gravels; gravel sand-clay mixtures
٠.	SW -	Well graded sands, sand-gravel mixtures
٠,`	SP.	Poorly groded sands
. : :	SM	
	SC.	Cloyey sonds, sond clay mixtures
•	ML	Silts, silty, very fine, sonds , sandy or clovey silts
	α,	Clays of low to medium plasticity; sitty, sandy or gravelly clay
-	CH.	Clays of high prosticity, for clays
	MH	Flastic siles uncocebus or diatomaceous siles
.7	OL .	Organic silts and organic silty clays of fow plasticity.
	CH.	Dragatic clays of sits of medium to high plasticity

8	Bosgl		- 12	Sc ?	Schist
	Gnais Gran				Shole :
٠.	Lime	stone"		S15	State State
Ma	Morb				Sondstone .

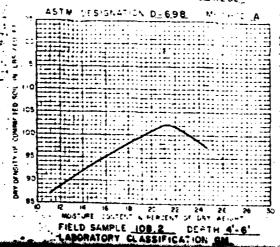
SAMPLES

D8 Disturbed

US Undisturbed

COMPACTION CURVE

LAMINATORY SAMPLE NO 73WEDR

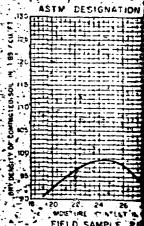


2501127-8

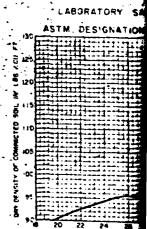


FIELD SAMPLE

COMPACTA LABORATORY SAL



COMPACT



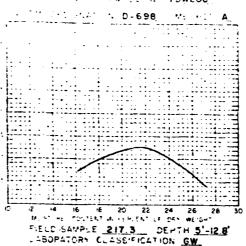
FIELD SAMPLE

##7.50 FAMELE NO 73W203 ES 3547 75 D-698 MATE TE CONTENT IN PERCENT OF THE WEIGHT SAMPLE 216.1 DEPTH 1.7'-6' ATORY CLASSIFICATION CL COMPACTION CURVE RATORY SAMPLE NO 73W204 \_ DESIGNATION D-968 24 26 .20 3C 32 34 36 M CONSTRUCT SERVICE OF DRY MEMOUT SAMPLE 217.1 DEPTH 4.3' COMPACTION CURVE ESIGNATION D-698 METHOD A

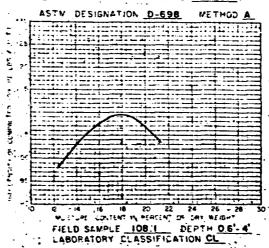
SONTENT IN PERCENT AT DAY OF SHE SAMPLE 217.2 DEPTH 3'-5' ATORY CLASSIFICATION GM

COMPACT ON CUEVE

COMPATTION CURVE CARCEATTER CAMPLE NO 73W206



COMPACTION CURVE



All soil and rock classifications were determined by visual examination.

NESHAMINY CREEK WATERSHED FLOODWATER RETARDING DAM PA - 615 BUCKS COUNTY, PENNSYLVANIA COMPACTION DATA

U. S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE

PLATE 15.

APPENDIX

F

### SITE GEOLOGY RAILROAD CREEK DAM

The Railroad Creek Dam is located in the Triassic Lowland Section of the Piedmont Physiographic Province. As shown in Plate F-1, the dam is underlain by the Triassic age Lockatong Formation which consists of gray or red argillite and siltstone. Immediately south of the dam lie shale and arkose of the Stockton Formation. These two rock formations are in fault contact with each other. The faults strikes near east-west passing near the right abutment and has been mapped for over a distance of 25 miles across Bucks and Montgomery Counties. Bedding in the emergency spillway area strikes west-northwest, dipping 40 degrees to the south (downstream direction). Rock jointing predominantly strikes to the north-east with high angle dips. Information contained in SCS files states that the dam in general is underlain by moderately soft argillite and siltstone weathered to a depth of less than ten to over 25 feet. The weathered rock was overlain by approximately 6 feet of residual soil. Localized swampy areas were described in the alluvial deposits of the flood plain.

